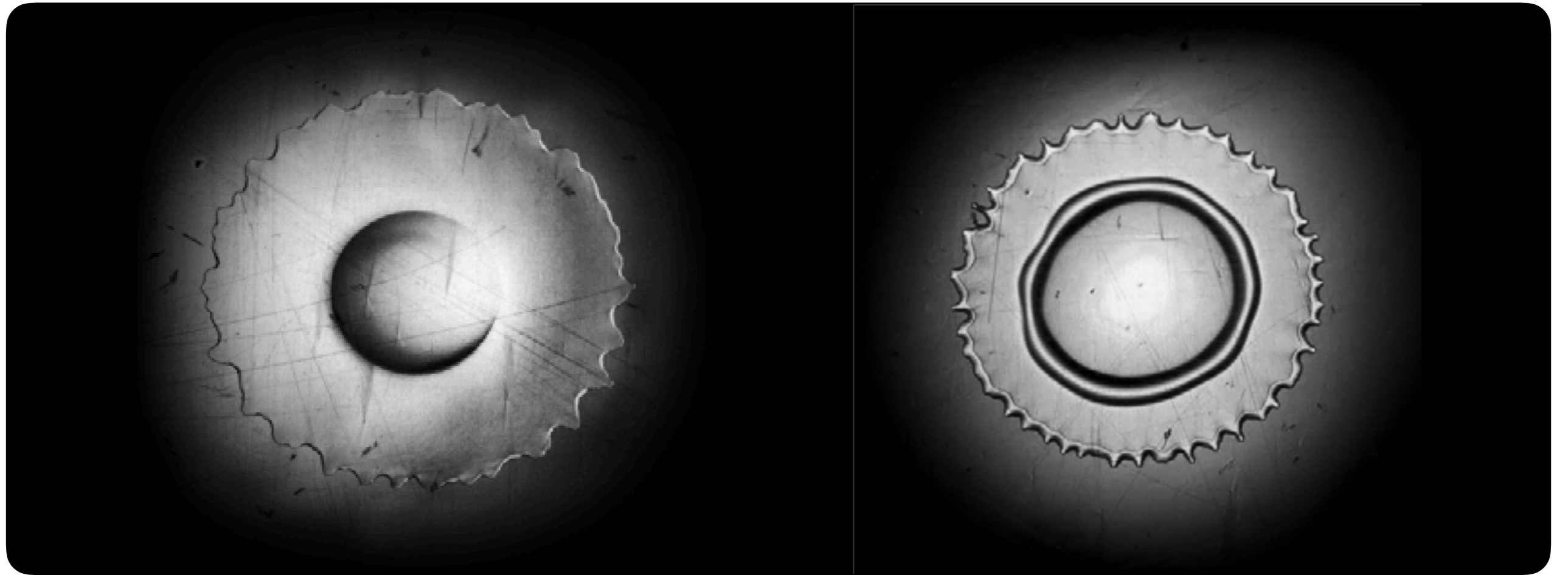


STORY OF A FREEZING DROP IMPACT



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(Institut d'Alembert, CNRS & UPMC, Paris, France)

Christophe Josserand

(LadHyX, École Polytechnique, Palaiseau)

CONTEXT IN ENVIRONMENT



Ice waterfall,
ice stalagmite,
icicle ...



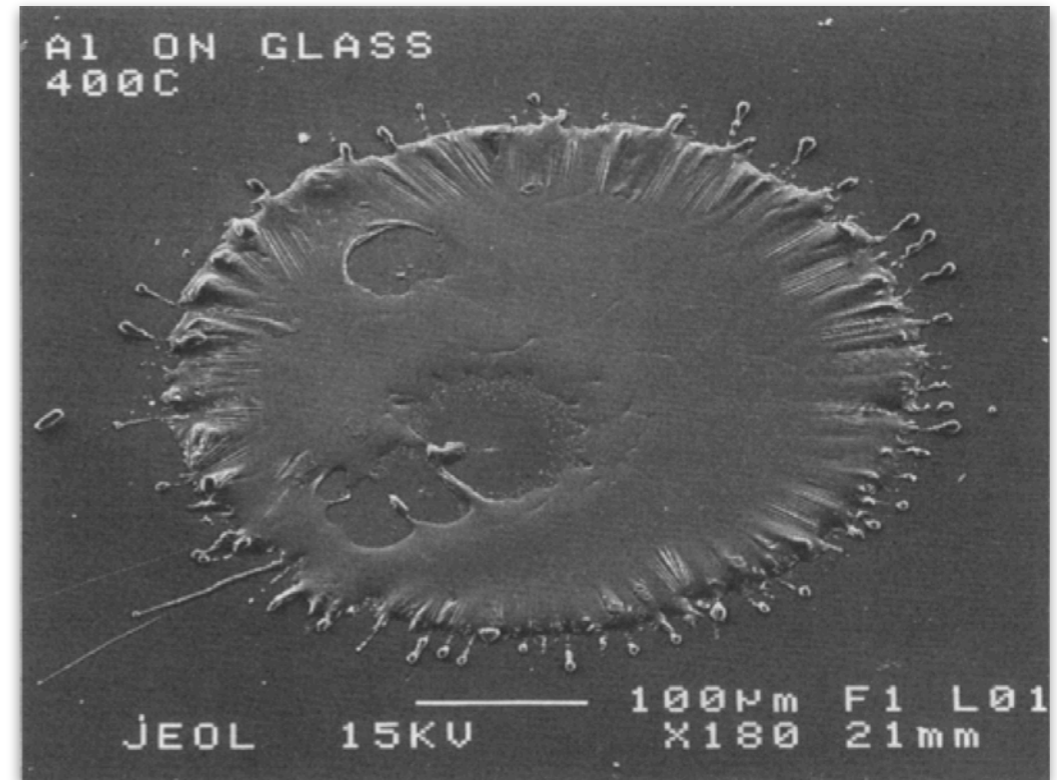
CONTEXT IN INDUSTRY

Ice accretion

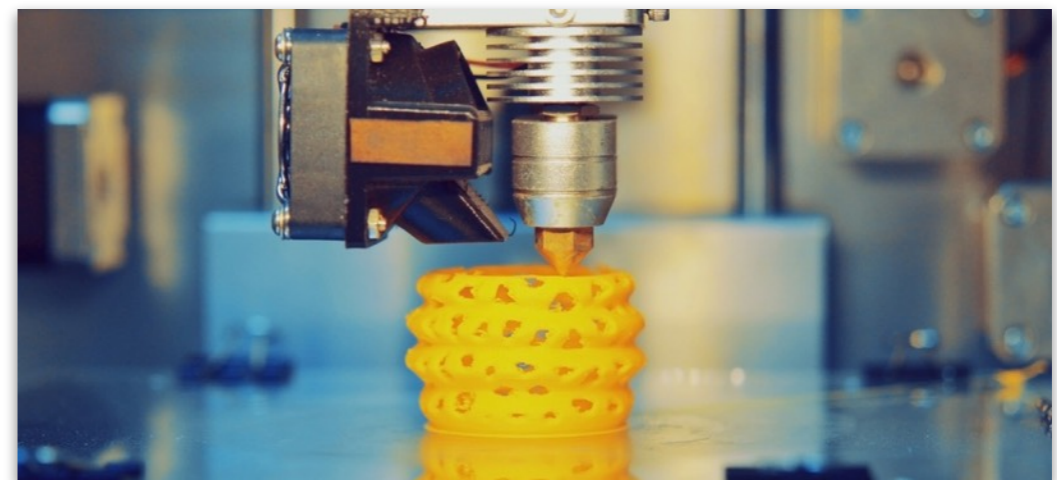


Aircraft icing (wings, pitot sensors ...)

Coating metallurgy

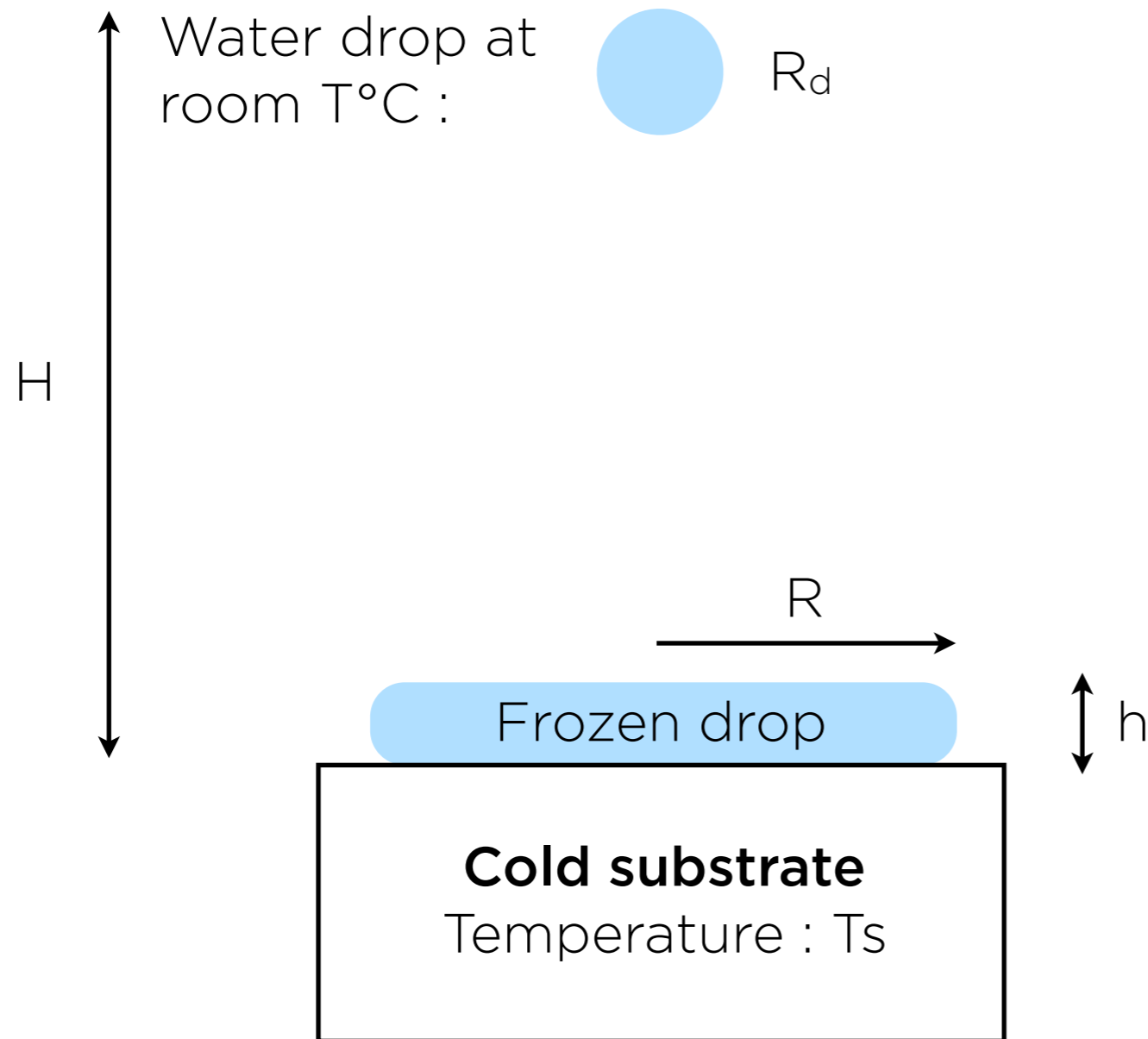


3D printing



Wind turbine

EXPERIMENTAL SETUP

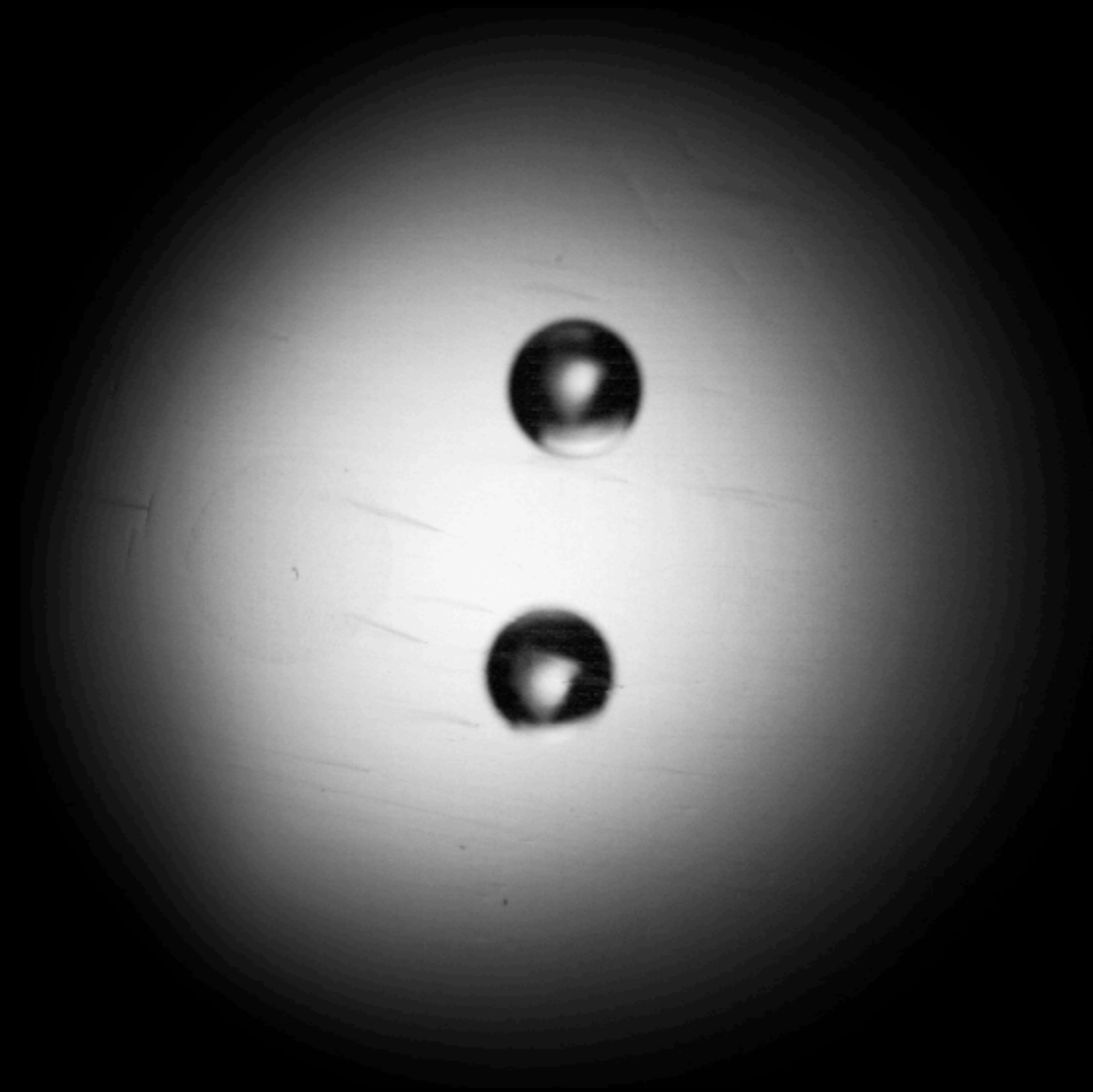


- High speed imaging
- Optical Profilometer
- Dry air at room $T^{\circ}\text{C}$

$H = 10 - 50 \text{ cm}$
 $R_d = 1 - 2 \text{ mm}$
 $T_s = 20 - \mathbf{-80^{\circ}\text{C}}$
Material : Cu,
steel, marble

$R \sim 10 \text{ mm}$
 $h \sim 0.2 \text{ mm}$

DROP IMPACT AT ROOM T°C



300x slower

Classic Impact

T = 20°C

DROP IMPACT AT ROOM T°C

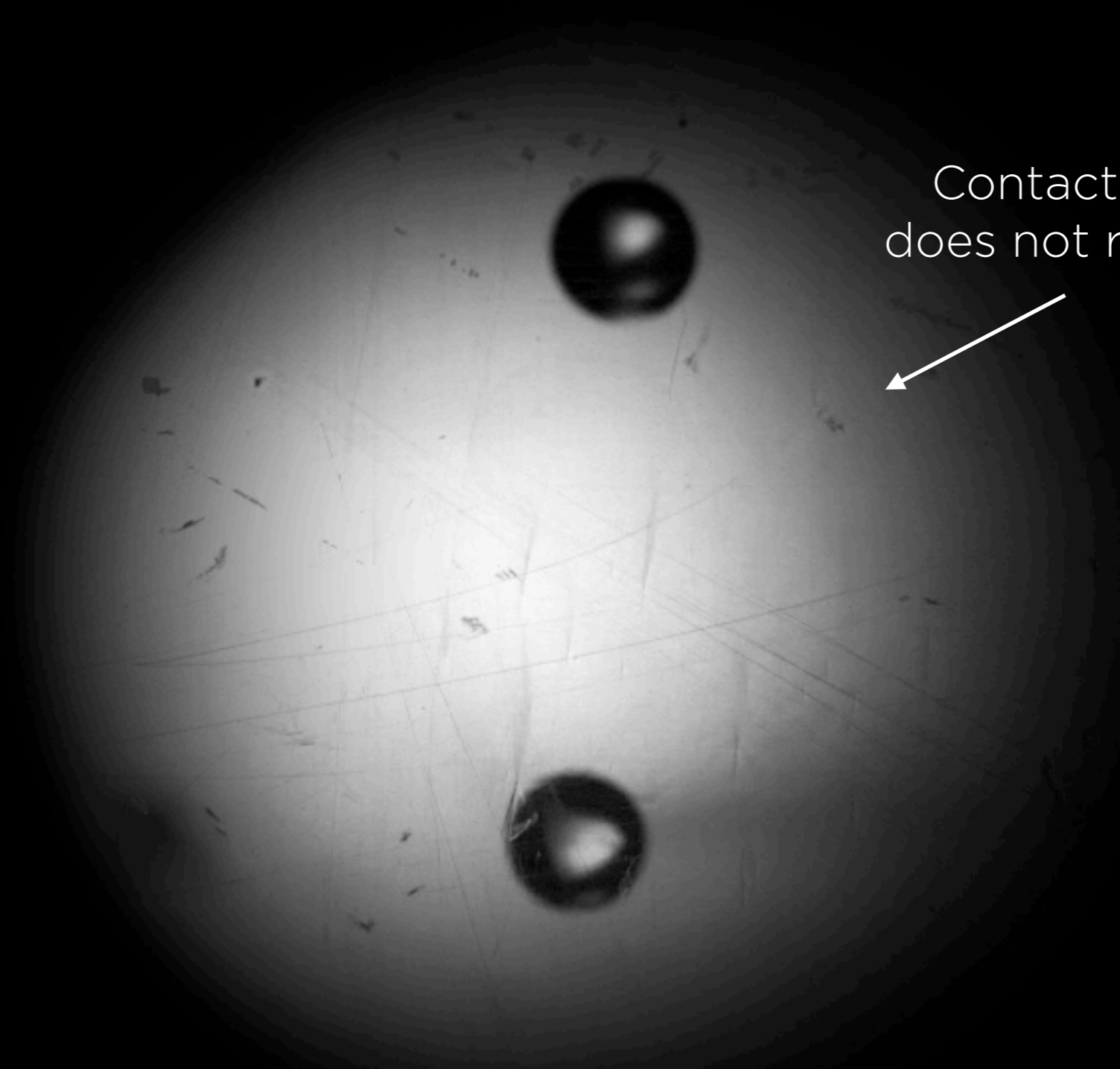


60x slower

Classic Impact

T = 20°C

IMPACT & FREEZING $T = -10^{\circ}\text{C}$



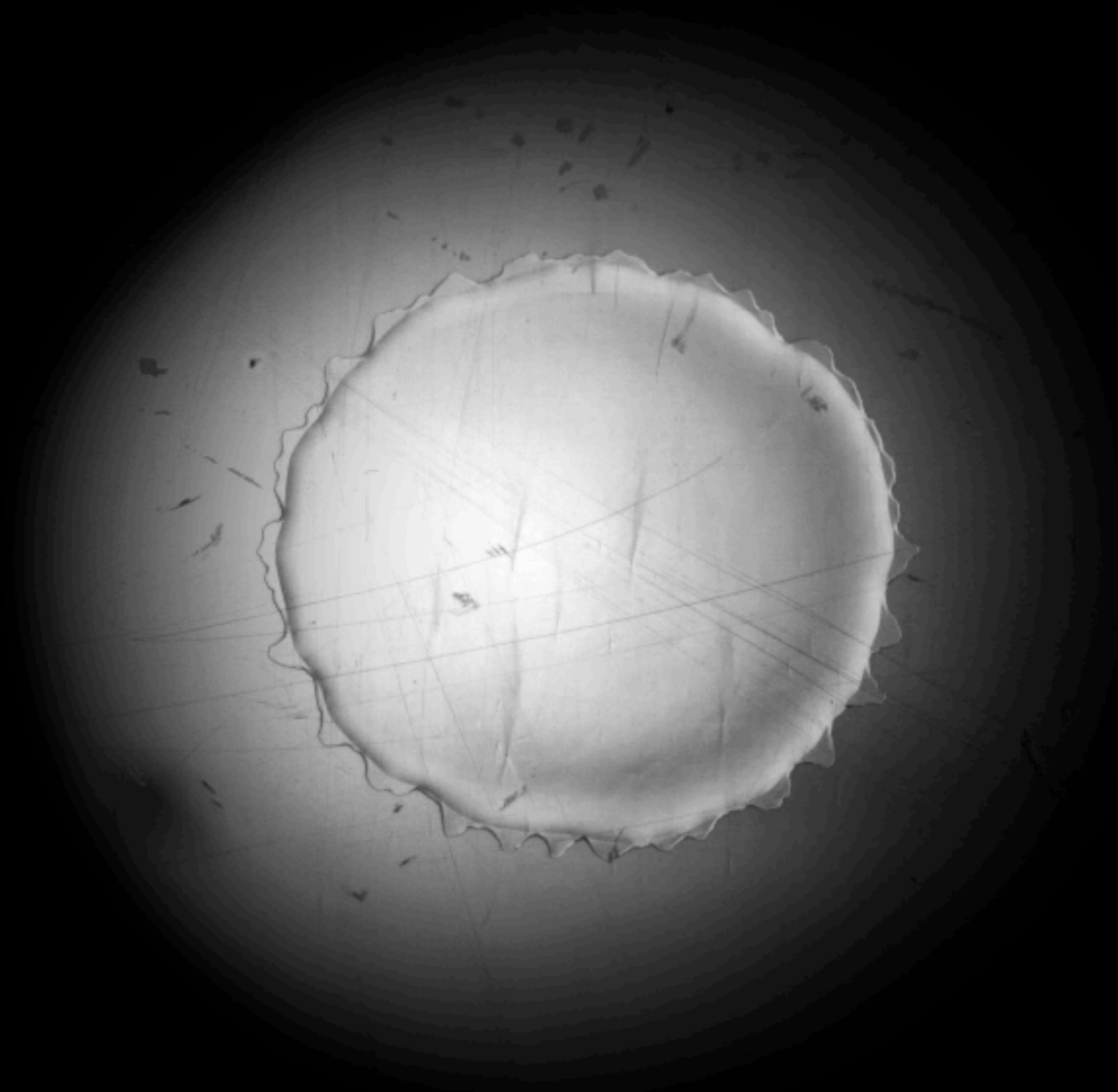
Contact line
does not retract



300x slower

$T = -10^{\circ}\text{C}$

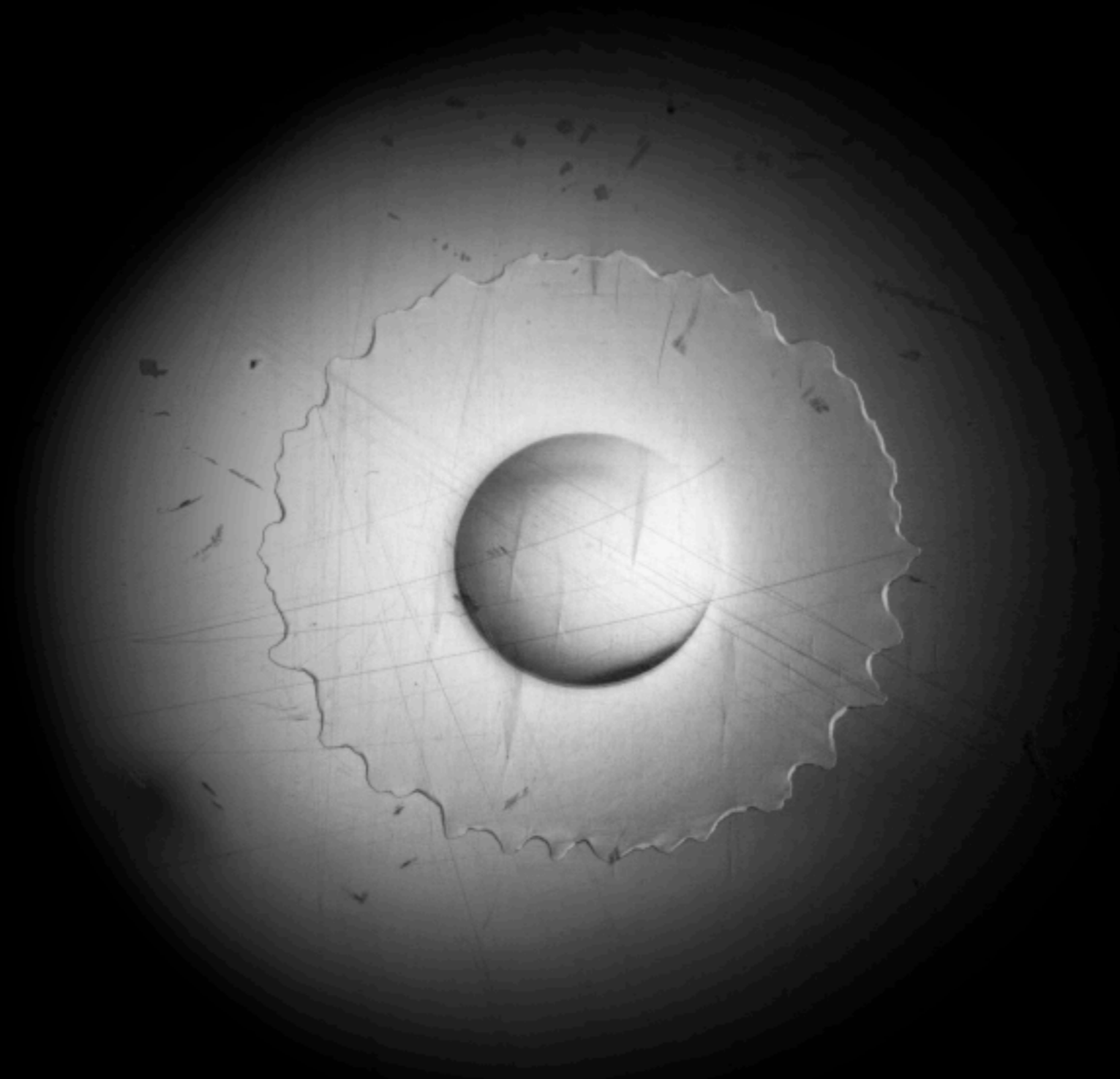
IMPACT & FREEZING $T = -10^{\circ}\text{C}$



50x slower

$T = -10^{\circ}\text{C}$

IMPACT & FREEZING $T = -10^{\circ}\text{C}$

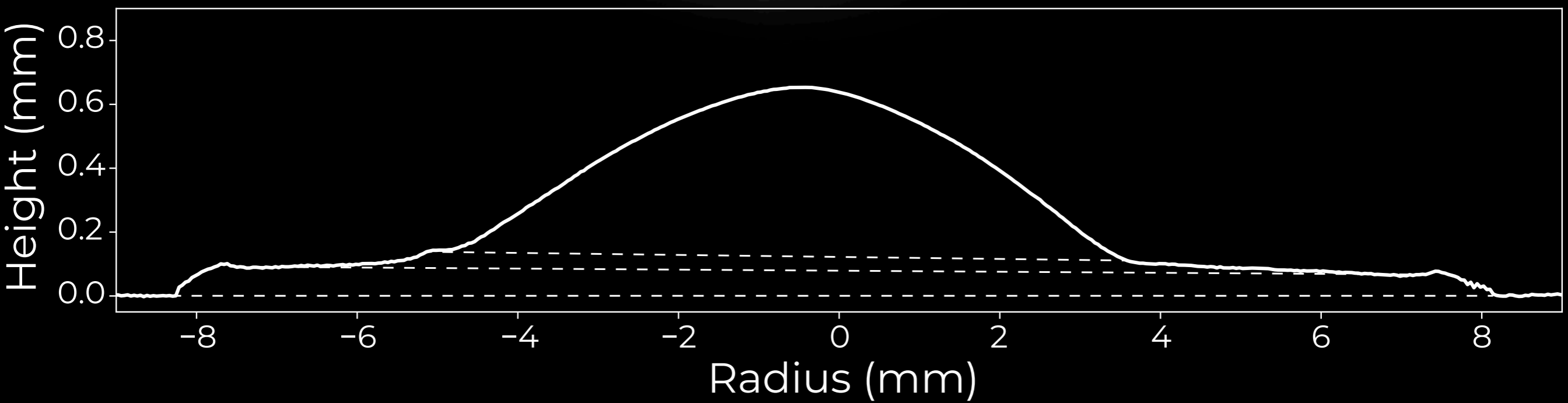
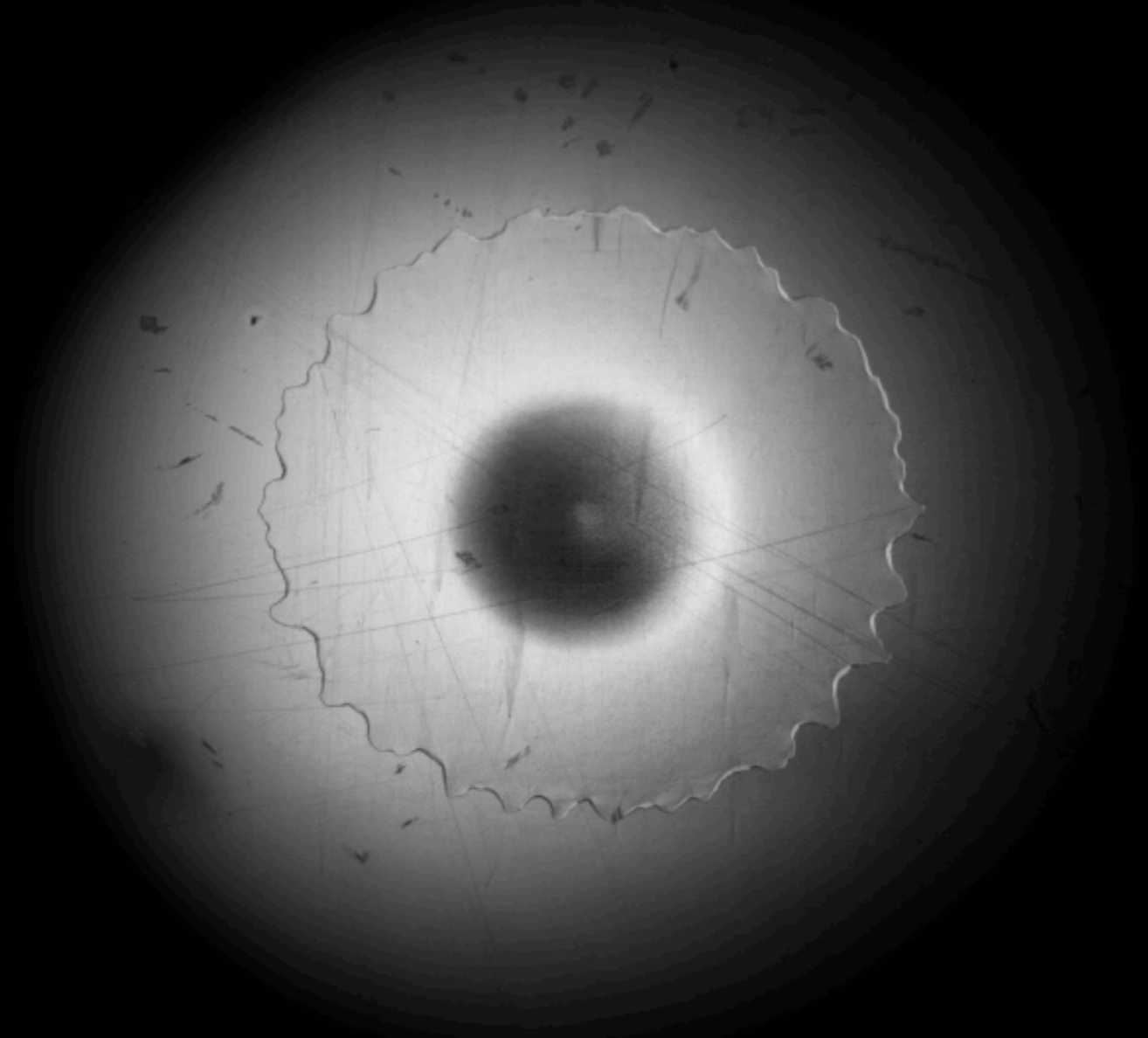


10x slower

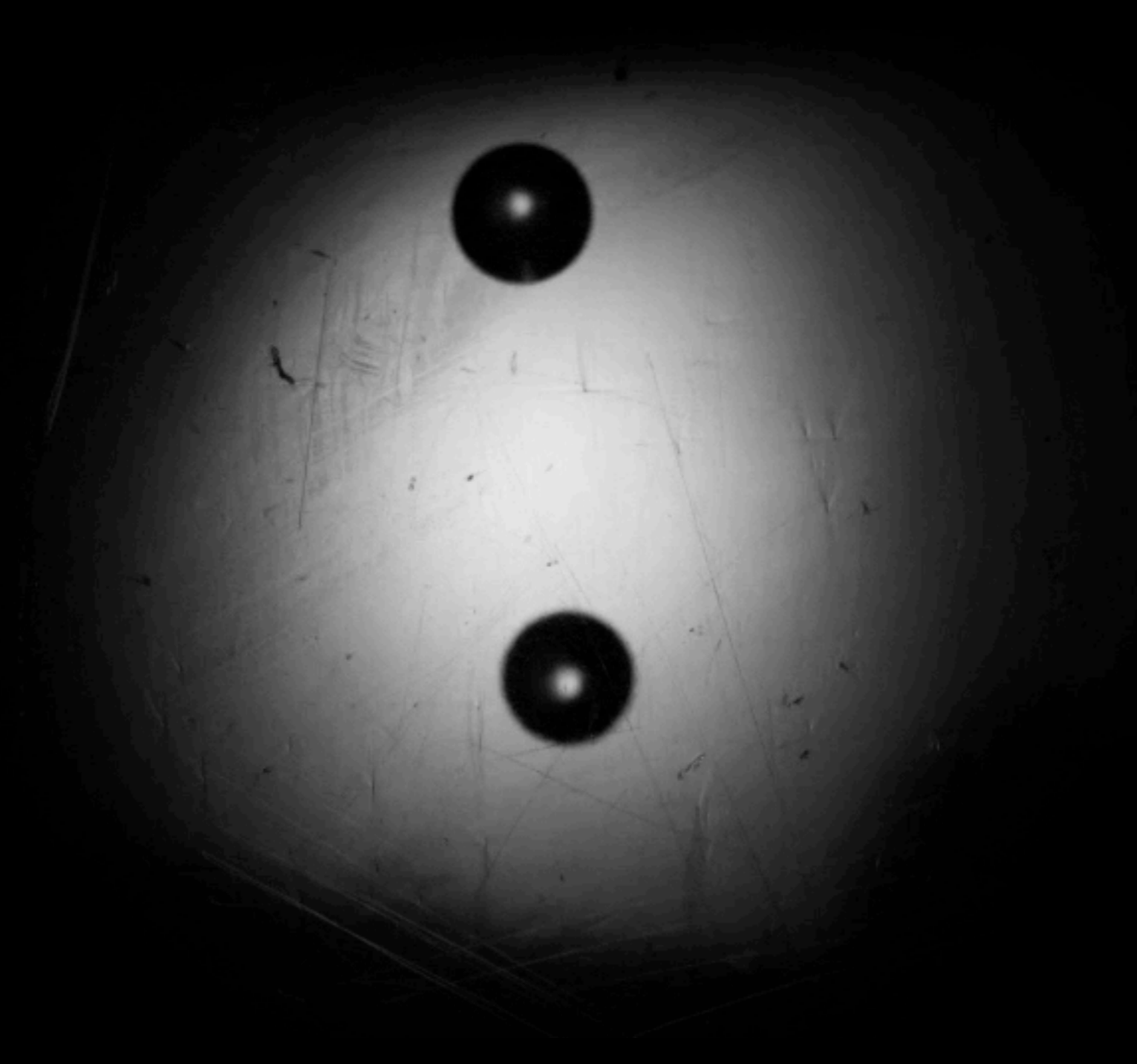
The Cap shape

$T = -10^{\circ}\text{C}$

IMPACT & FREEZING $T=-10^{\circ}\text{C}$



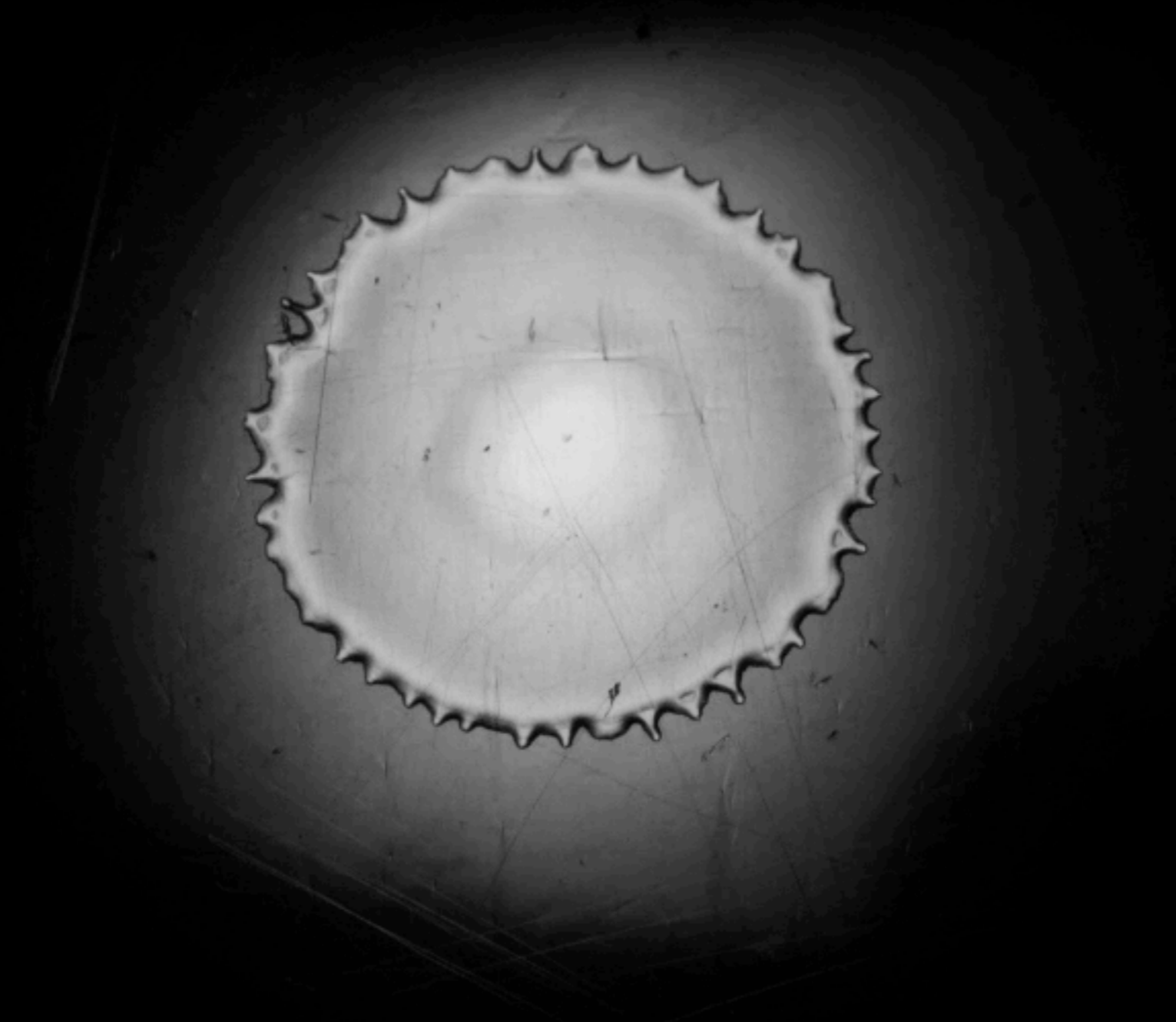
IMPACT & FREEZING $T = -30^{\circ}\text{C}$



200x slower

$T = -30^{\circ}\text{C}$

IMPACT & FREEZING $T = -30^{\circ}\text{C}$

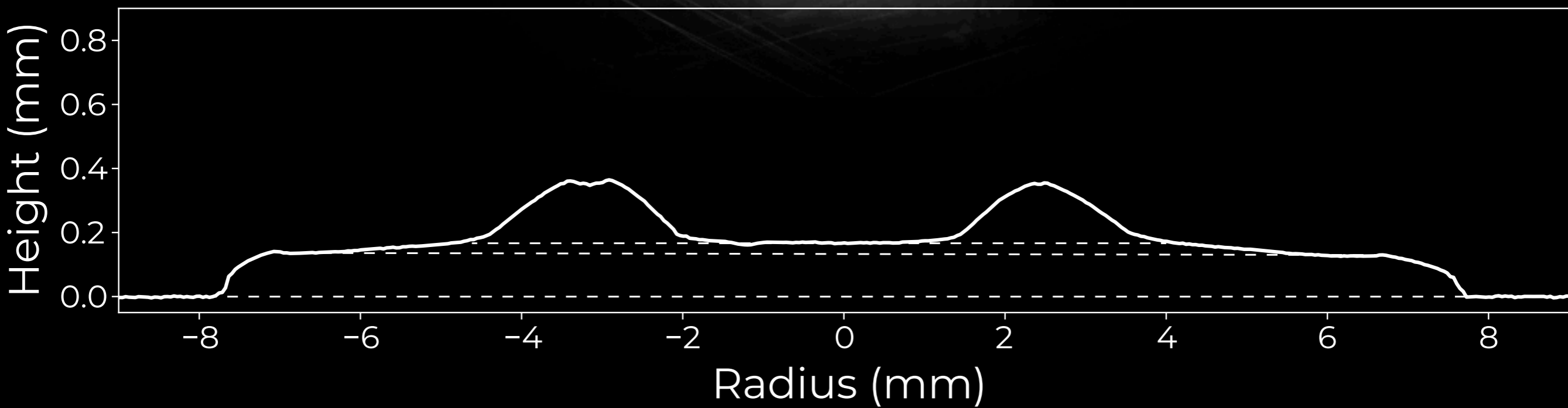
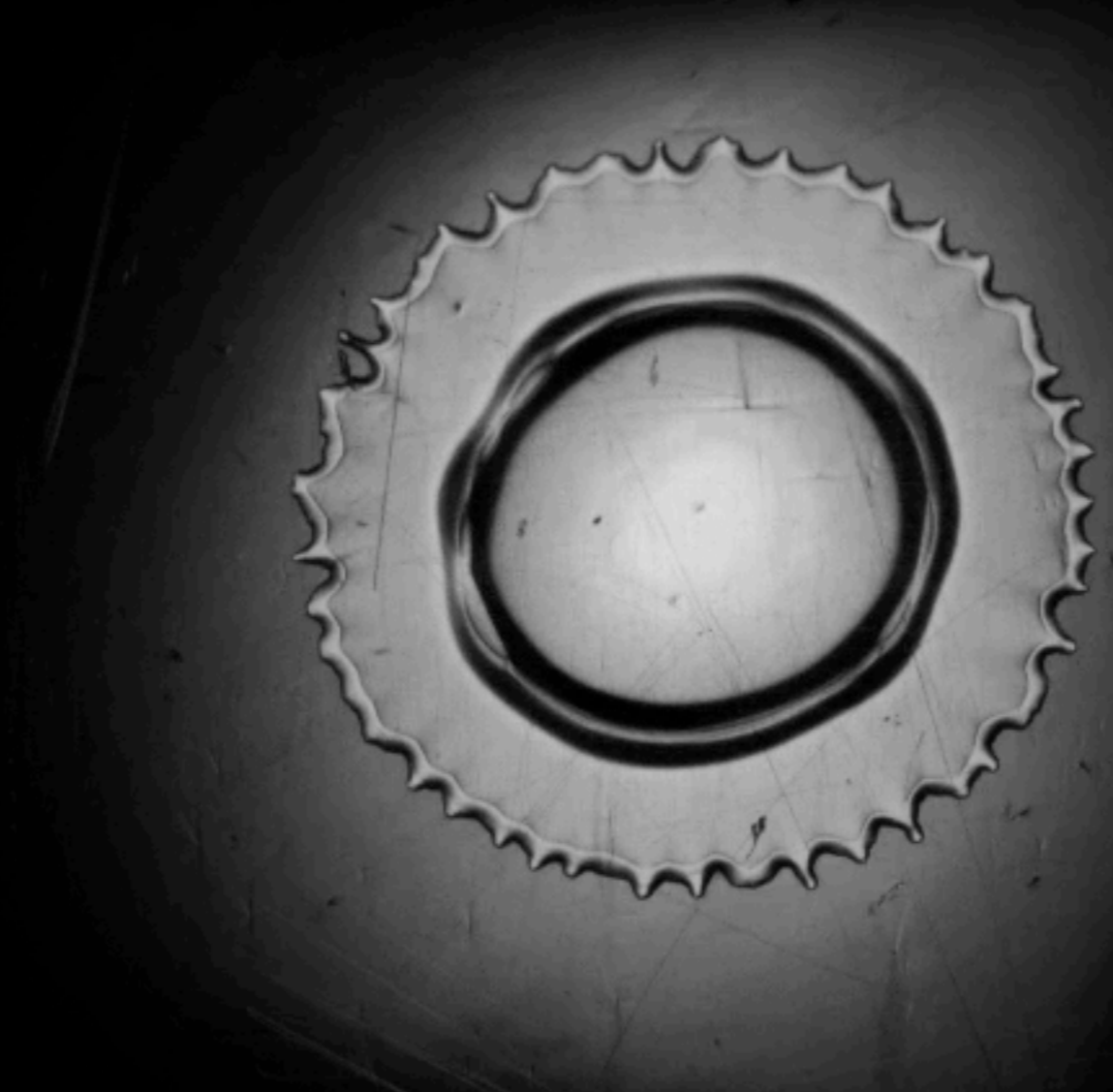


30x slower

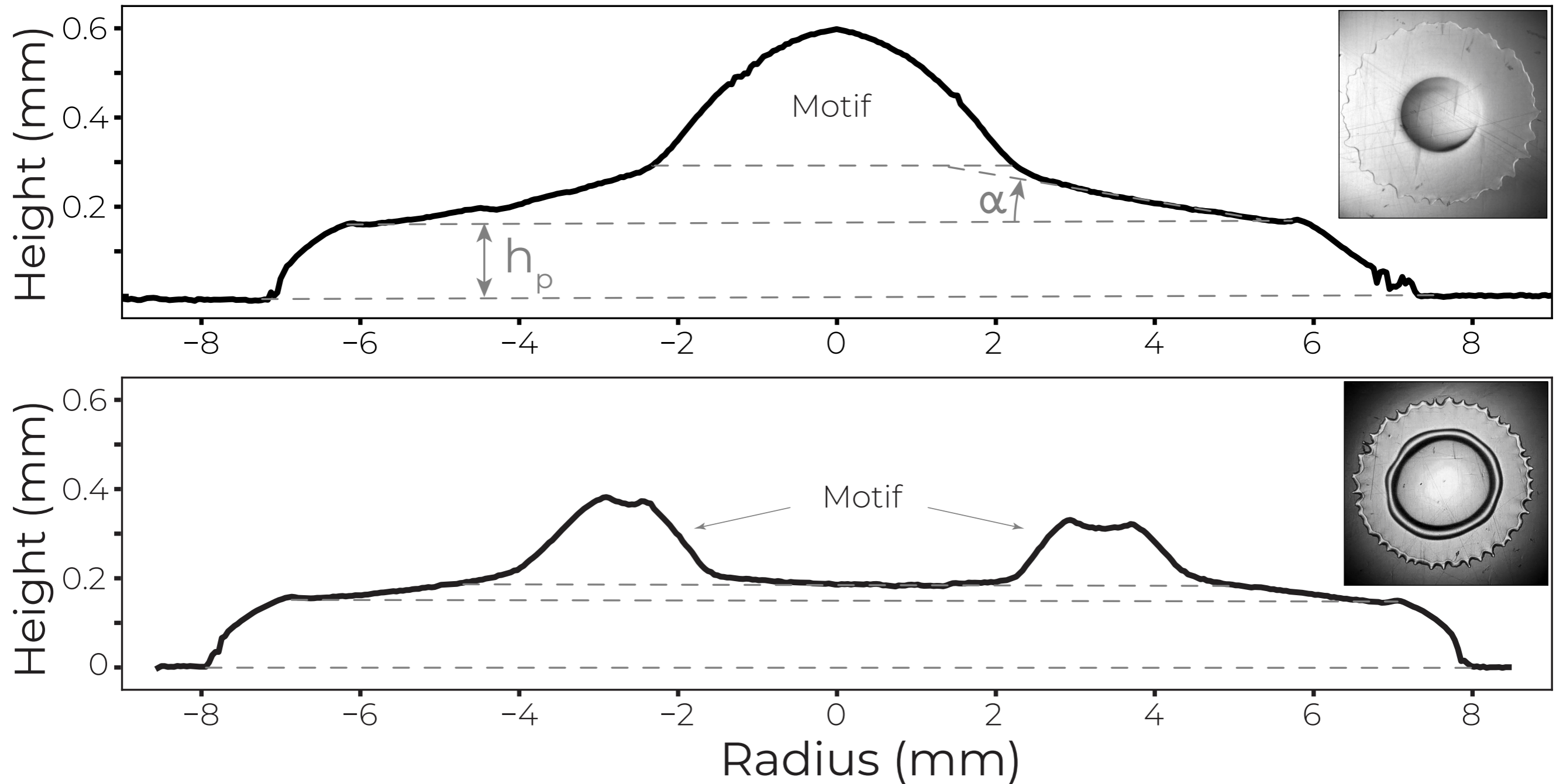
The Ring shape

$T = -30^{\circ}\text{C}$

IMPACT & FREEZING $T=-30^{\circ}\text{C}$



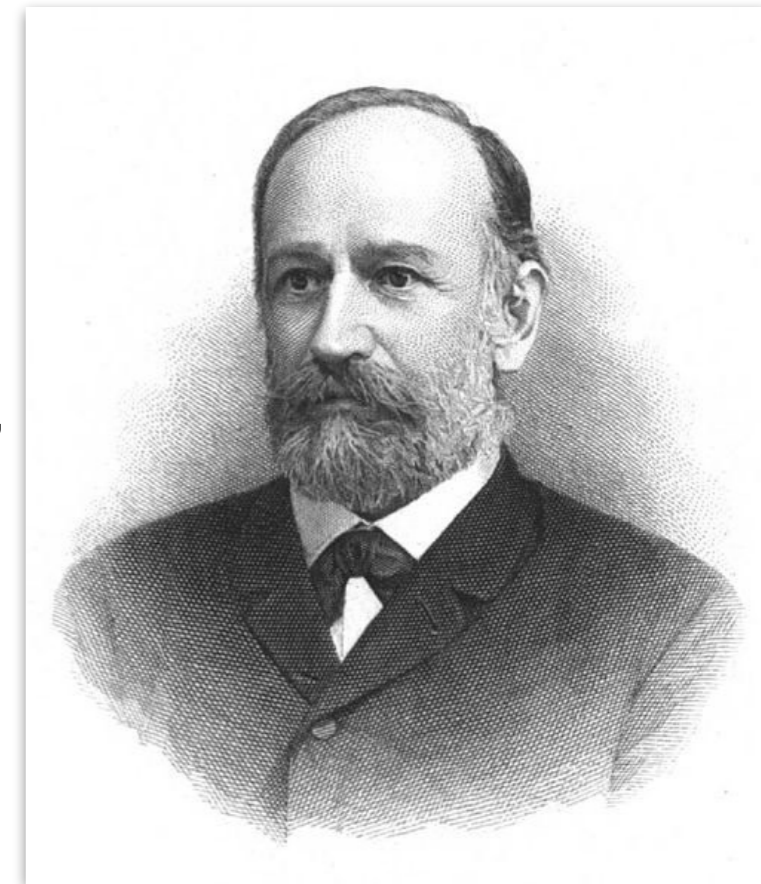
SHAPE OF A FROZEN DROP



● Can we understand and predict the shape of these particular ice structures ?

STEFAN PROBLEM (1889)

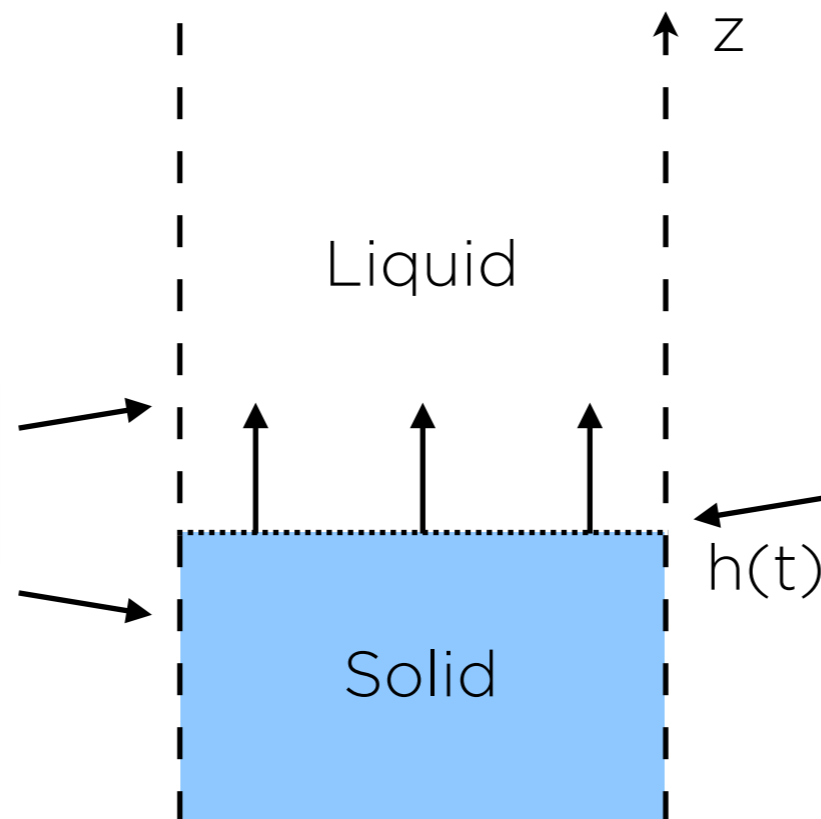
Josef Stefan



1835-1893

● The **classical Stefan problem** aims to describe an homogeneous medium undergoing a phase change (ice - water) by solving the **heat equation** and the **Stefan condition**, on the evolving boundary. In 1D :

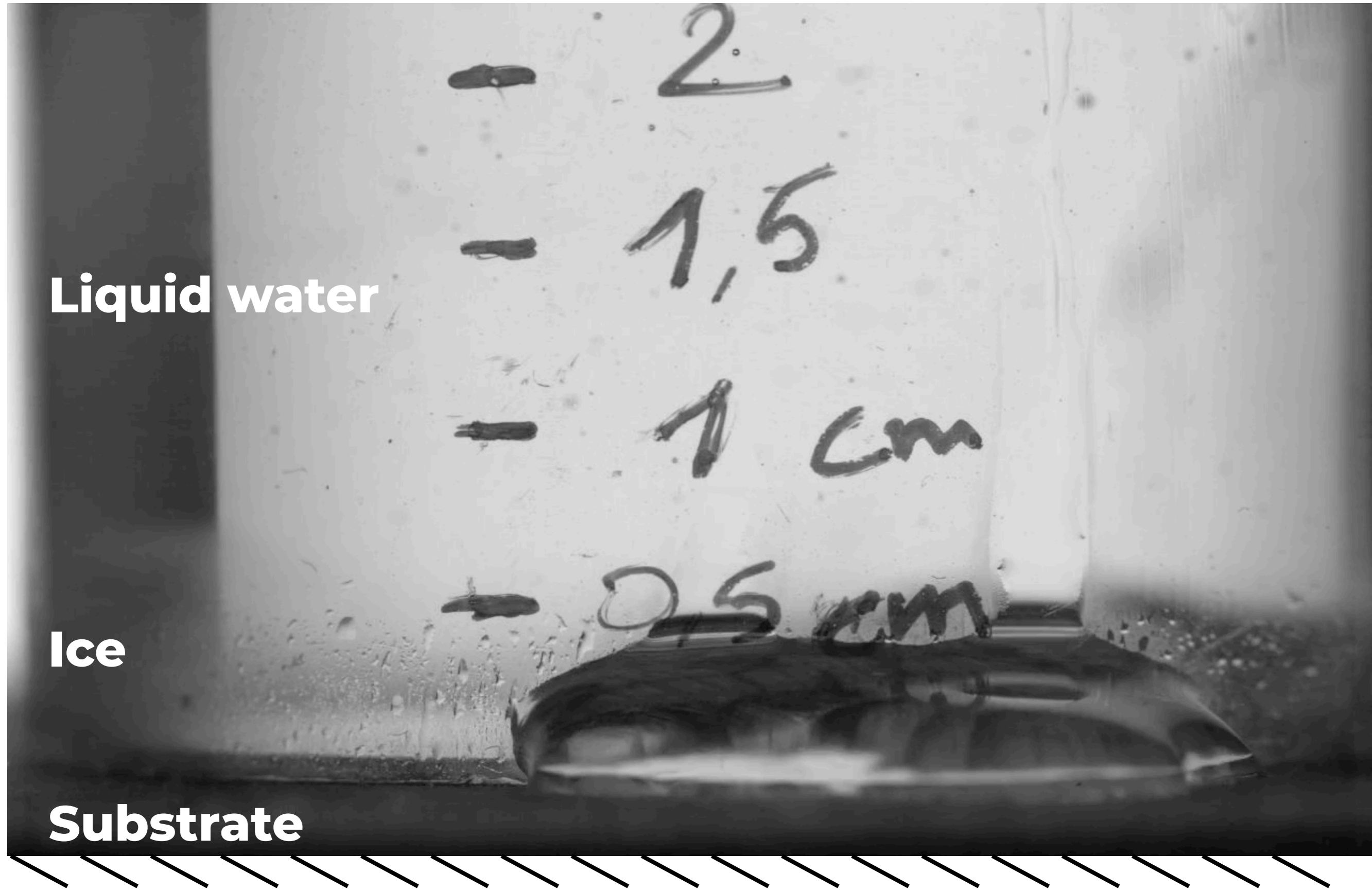
$$\frac{\partial T(z, t)}{\partial t} = D \frac{\partial^2 T(z, t)}{\partial z^2}$$



$$\rho_s L \frac{dh}{dt} = \lambda_s \frac{\partial T_s}{\partial z} - \lambda_l \frac{\partial T_l}{\partial z}$$

$$h(t) = \sqrt{D_{\text{eff}} t}$$

OUR STEFAN PROBLEM



Liquid water

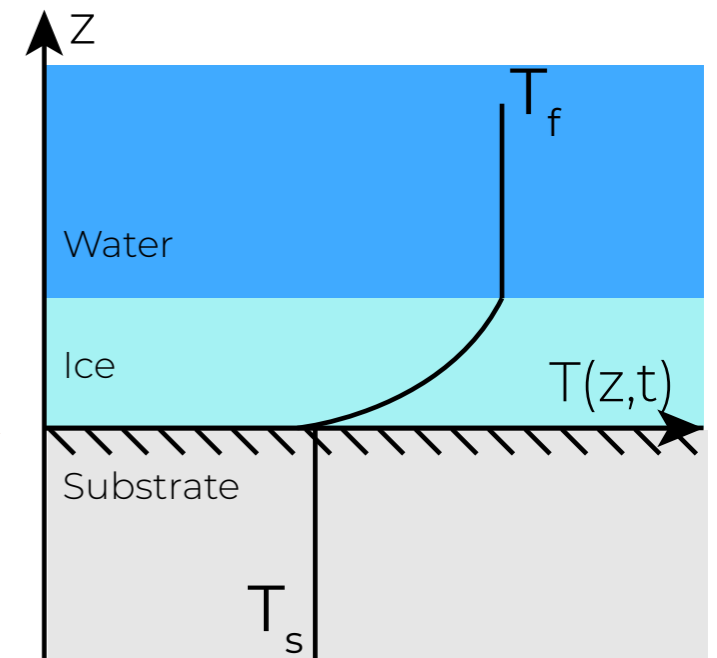
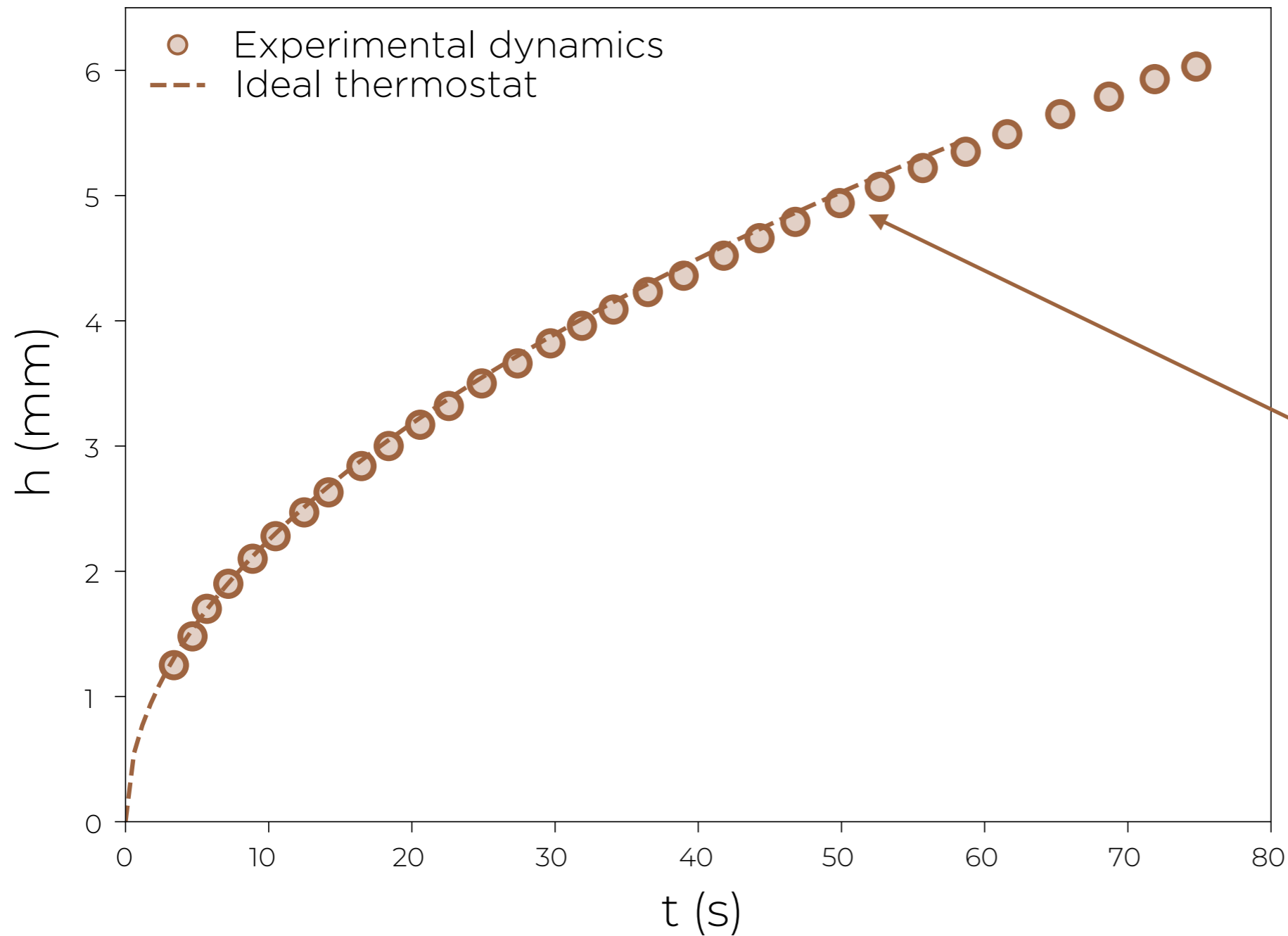
Ice

Substrate

2.
1,5
1 cm
0,5 cm

COMPARISON WITH STEFAN

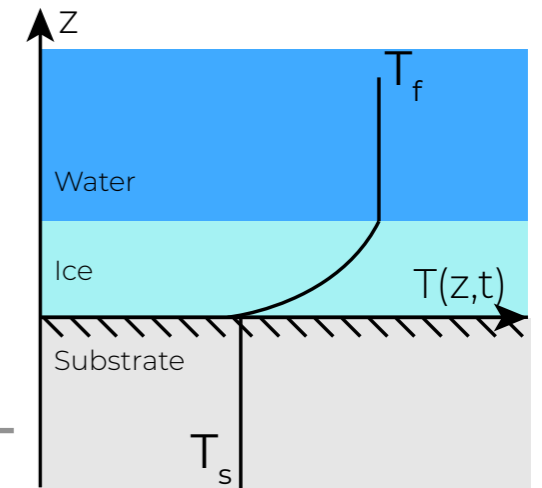
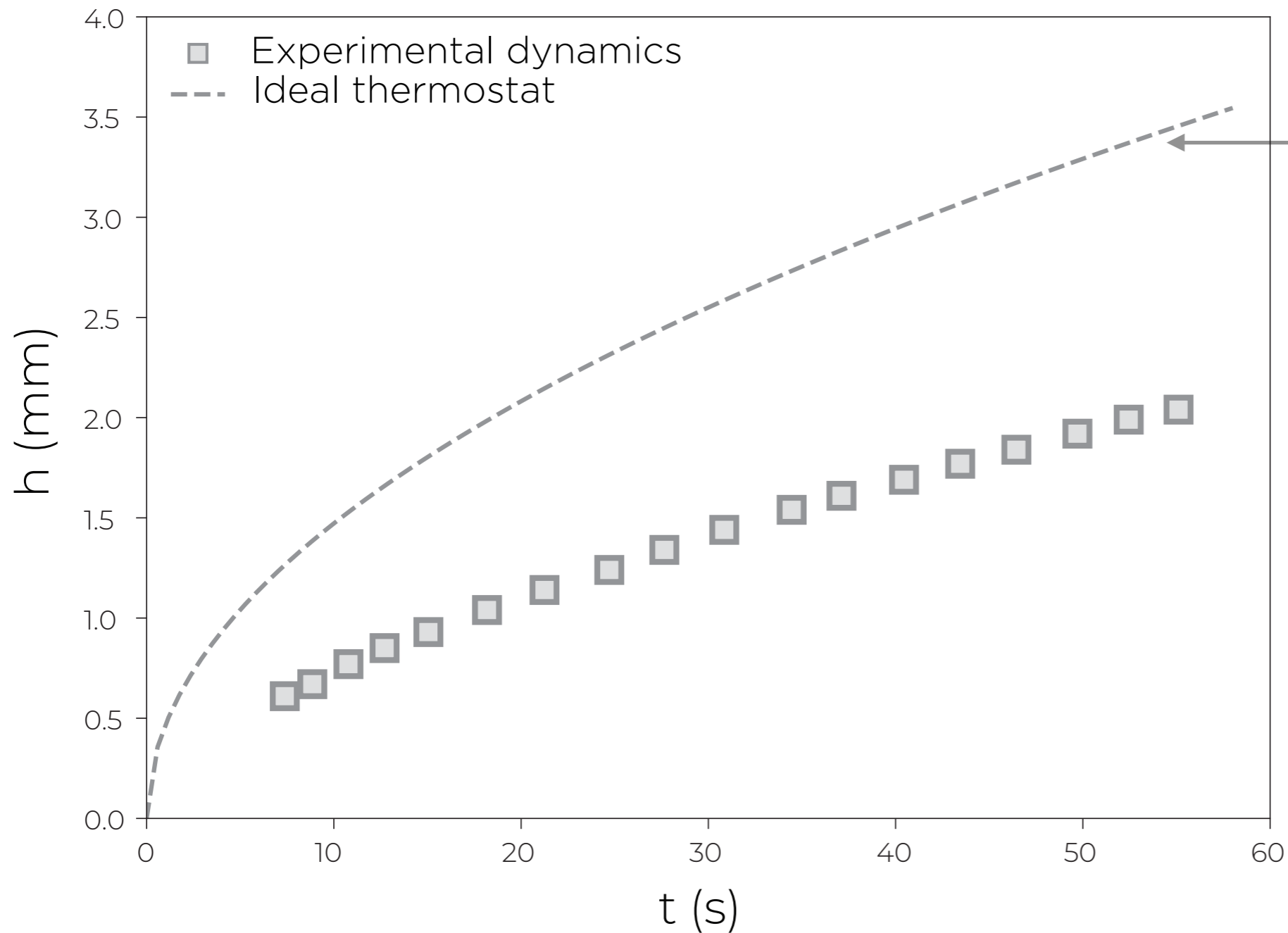
● Solidification of a water column on a **copper** substrate



Classical Stefan problem.
The substrate is an **ideal thermostat**

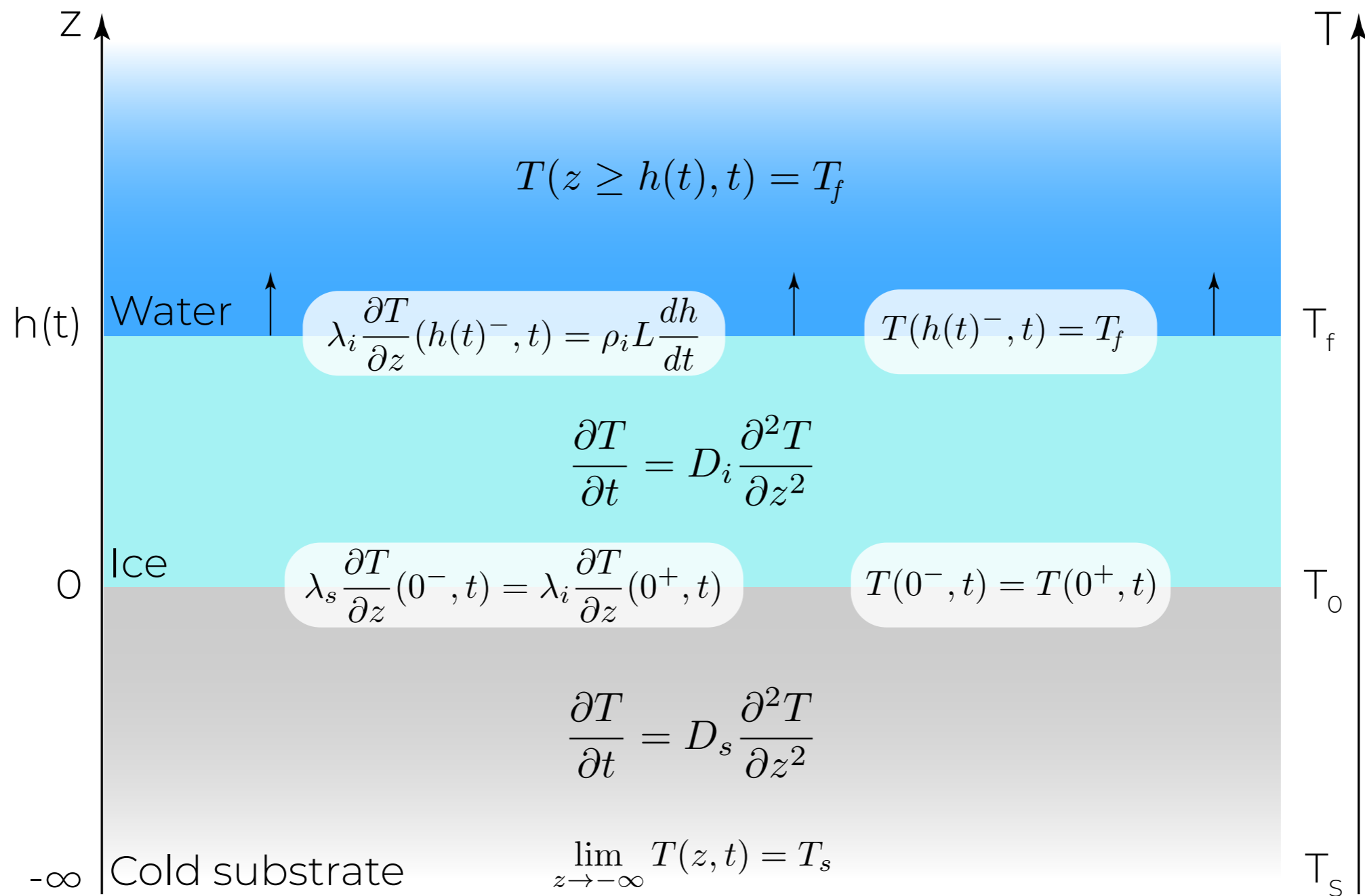
COMPARISON WITH STEFAN

● Solidification of a water column on a **steel** substrate



Classical Stefan problem.
The substrate is an
ideal thermostat

NEW SOLIDIFICATION MODEL

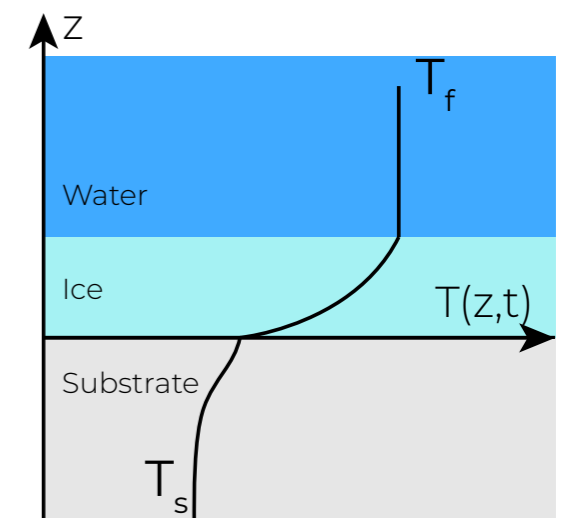
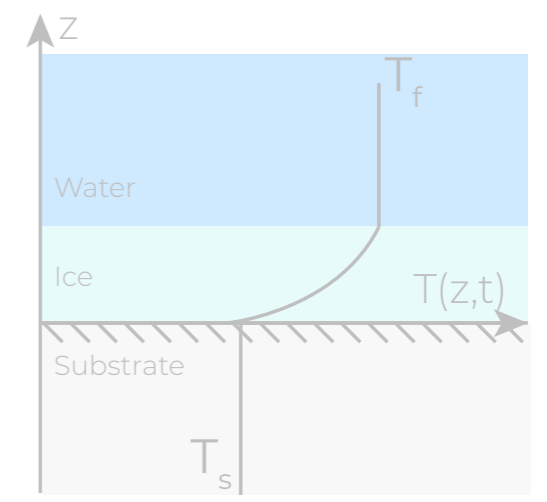
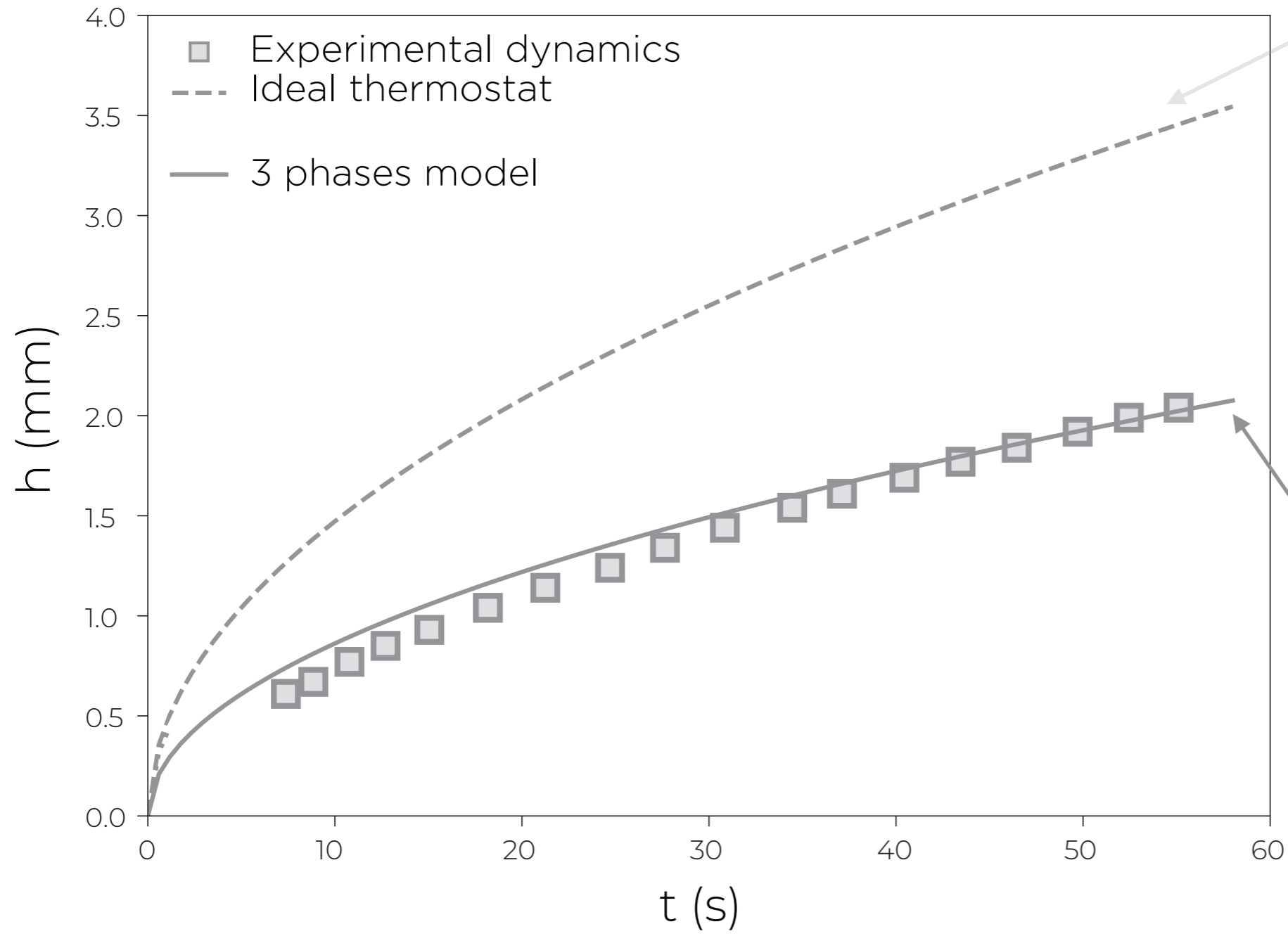


● Self-similar growth : $h(t) = \sqrt{D_{\text{eff}} t}$

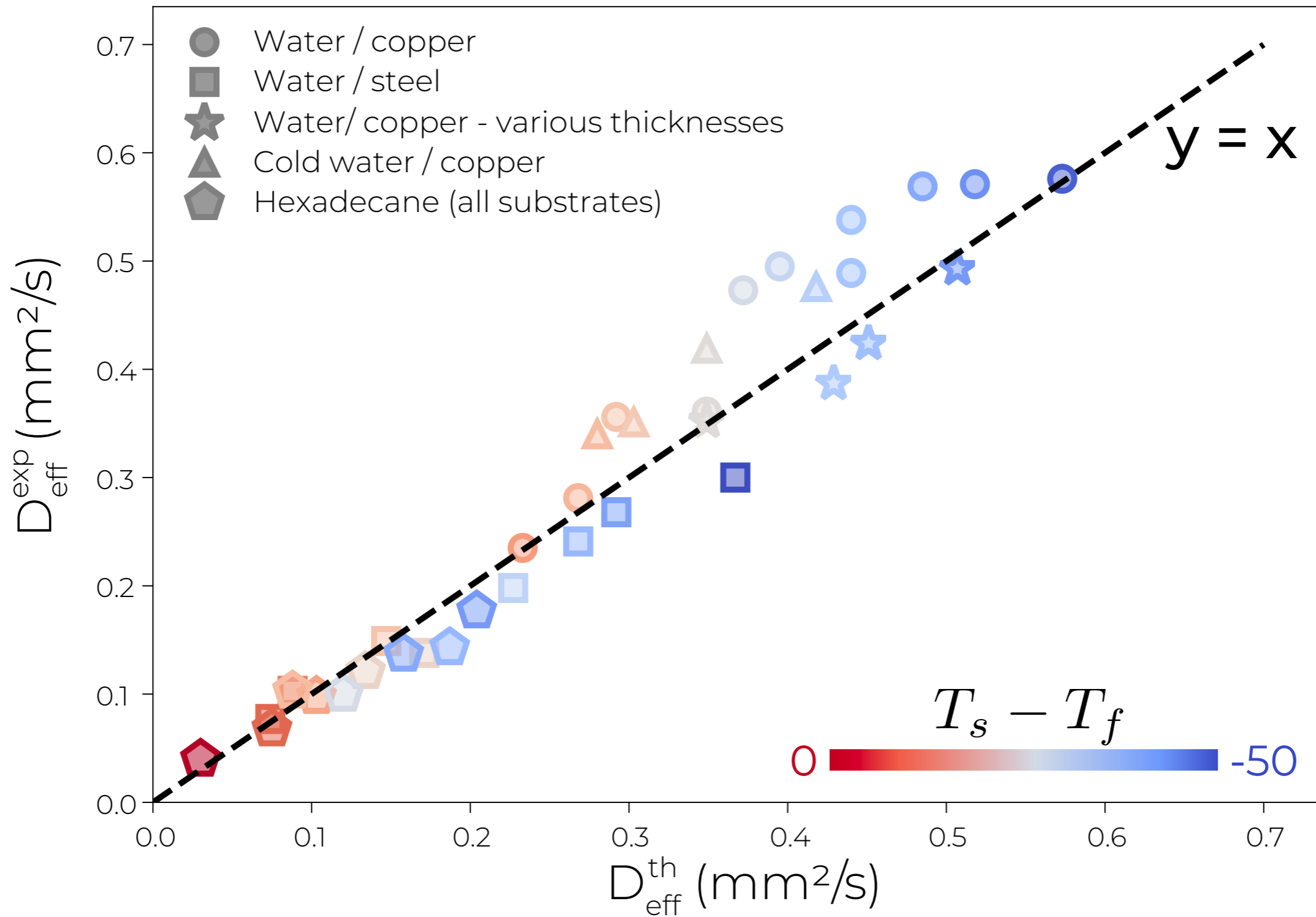
● D_{eff} depends on the thermal parameters of the system (ice & substrate).

COMPARISON WITH OUR 3 PHASES MODEL

● Solidification of a water column on a **steel** substrate

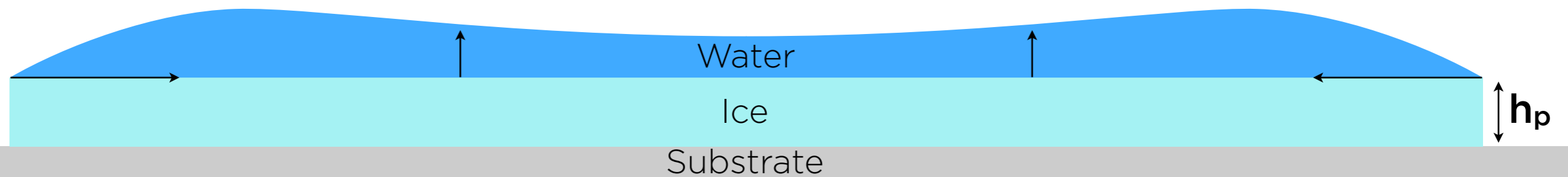


COMPARISON WITH OUR 3 PHASES MODEL



ICE PANCAKE THICKNESS

$$h(t) = \sqrt{D_{\text{eff}} t}$$

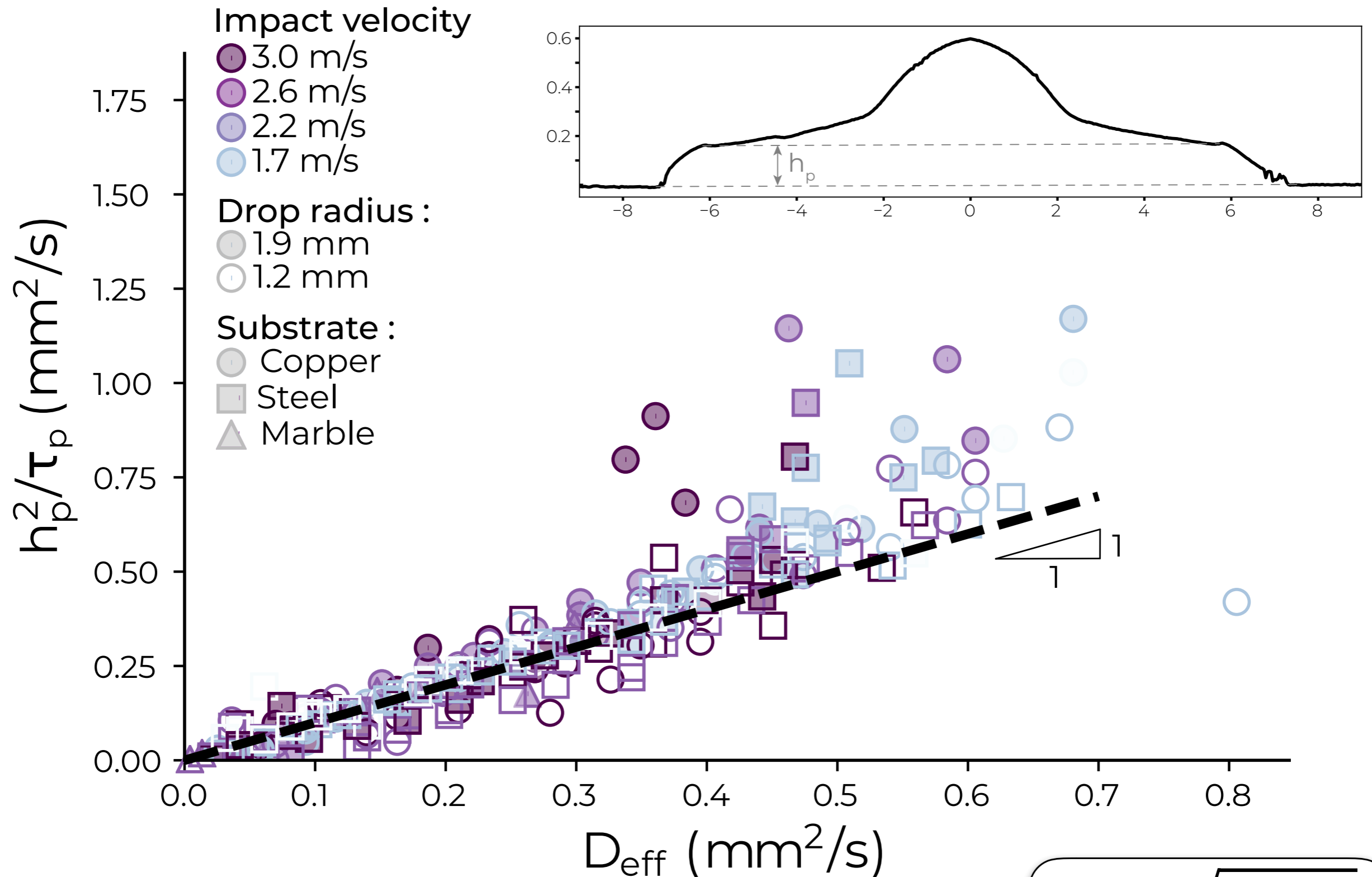


$$\text{Finally : } h_p = \sqrt{D_{\text{eff}} \tau_p}$$

?

● Ice pancake thickness h_p , with τ_p the solidification time before retraction.

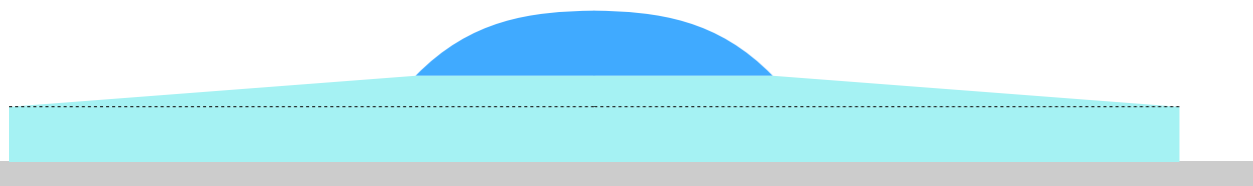
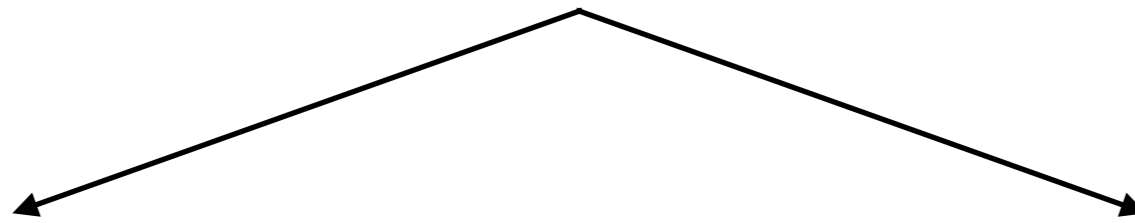
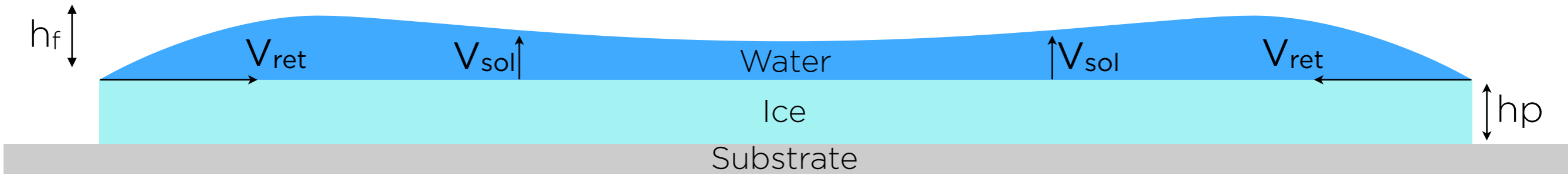
ICE PANCAKE THICKNESS



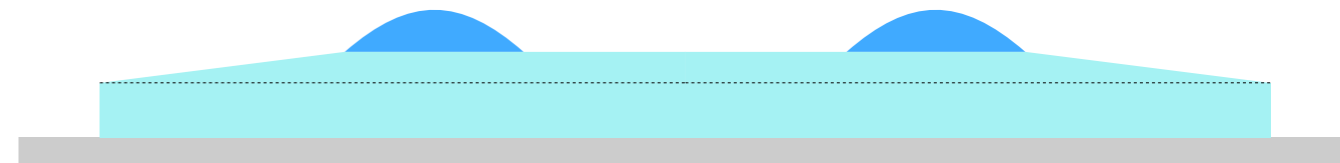
● Pancake thickness obey to a 1D heat propagation model and is built during contact line relaxation

$$h_p \approx \sqrt{D_{\text{eff}} \tau_p}$$

RETRACTION VS FREEZING

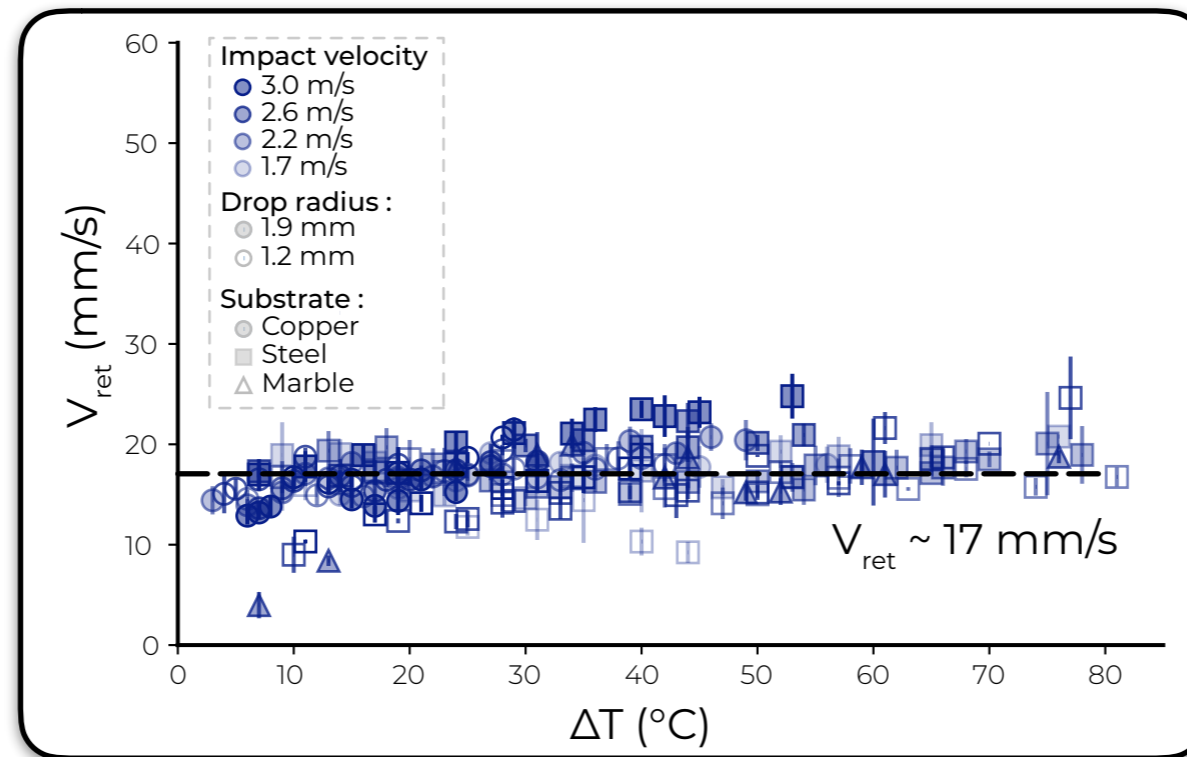
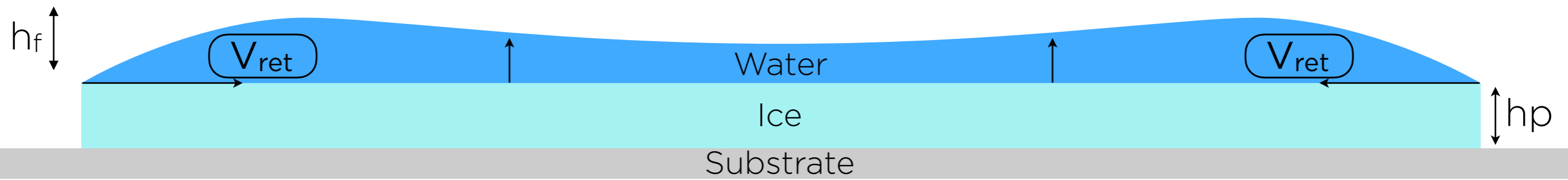


retraction time \ll solidification time



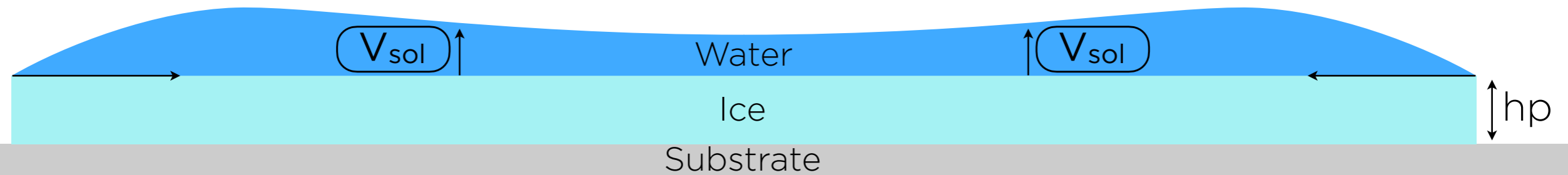
retraction time \gg solidification time

RETRACTION VELOCITY



Constant retraction velocity : $V_{ret} \simeq (2.3 \times 10^{-4}) \frac{\gamma}{\mu}$

SOLIDIFICATION VELOCITY



We have

$$h(t) = \sqrt{D_{eff}t}$$

so

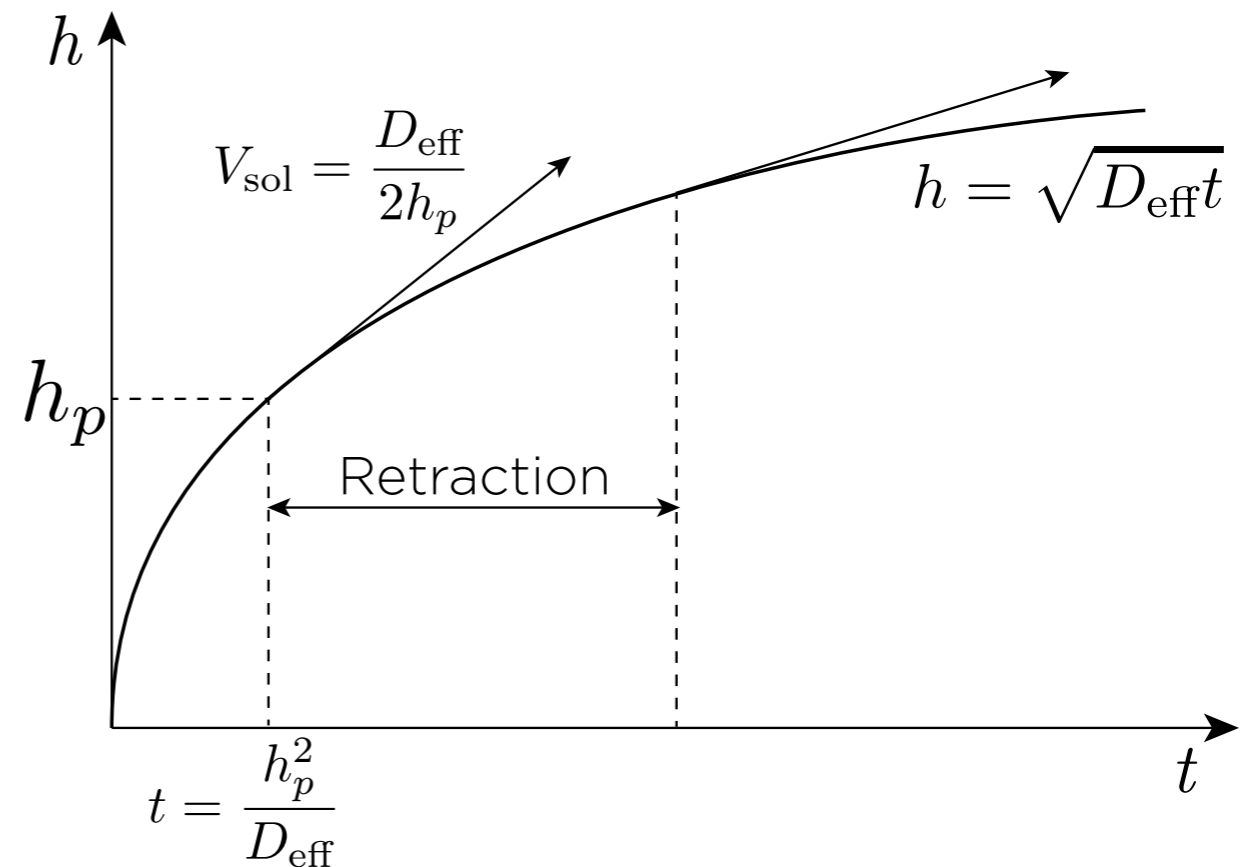
$$\frac{dh}{dt} = \frac{1}{2} \sqrt{\frac{D_{eff}}{t}}$$

at

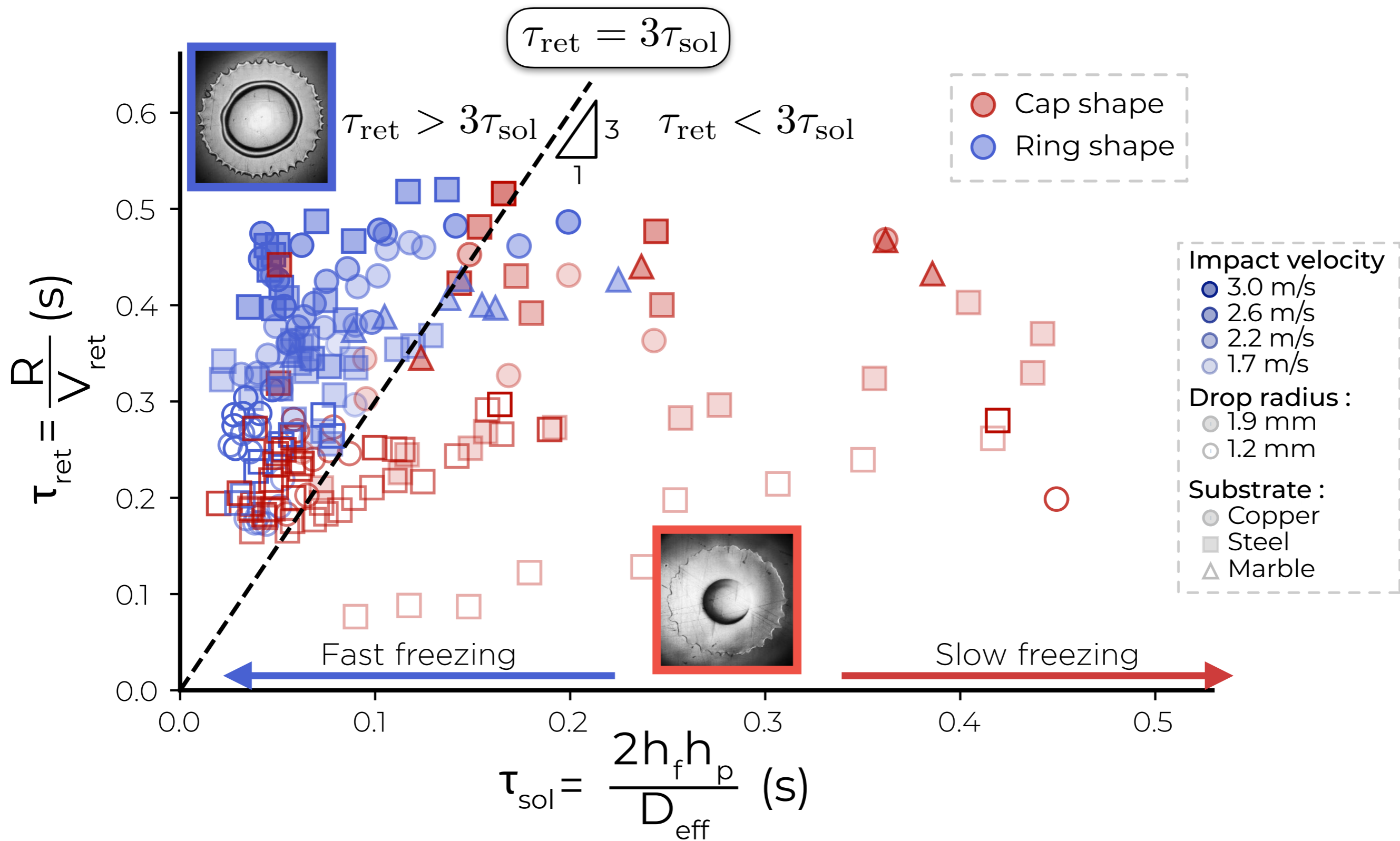
$$t = \frac{h_p^2}{D_{eff}}$$

we obtain

$$V_{sol} = \frac{D_{eff}}{2h_p}$$

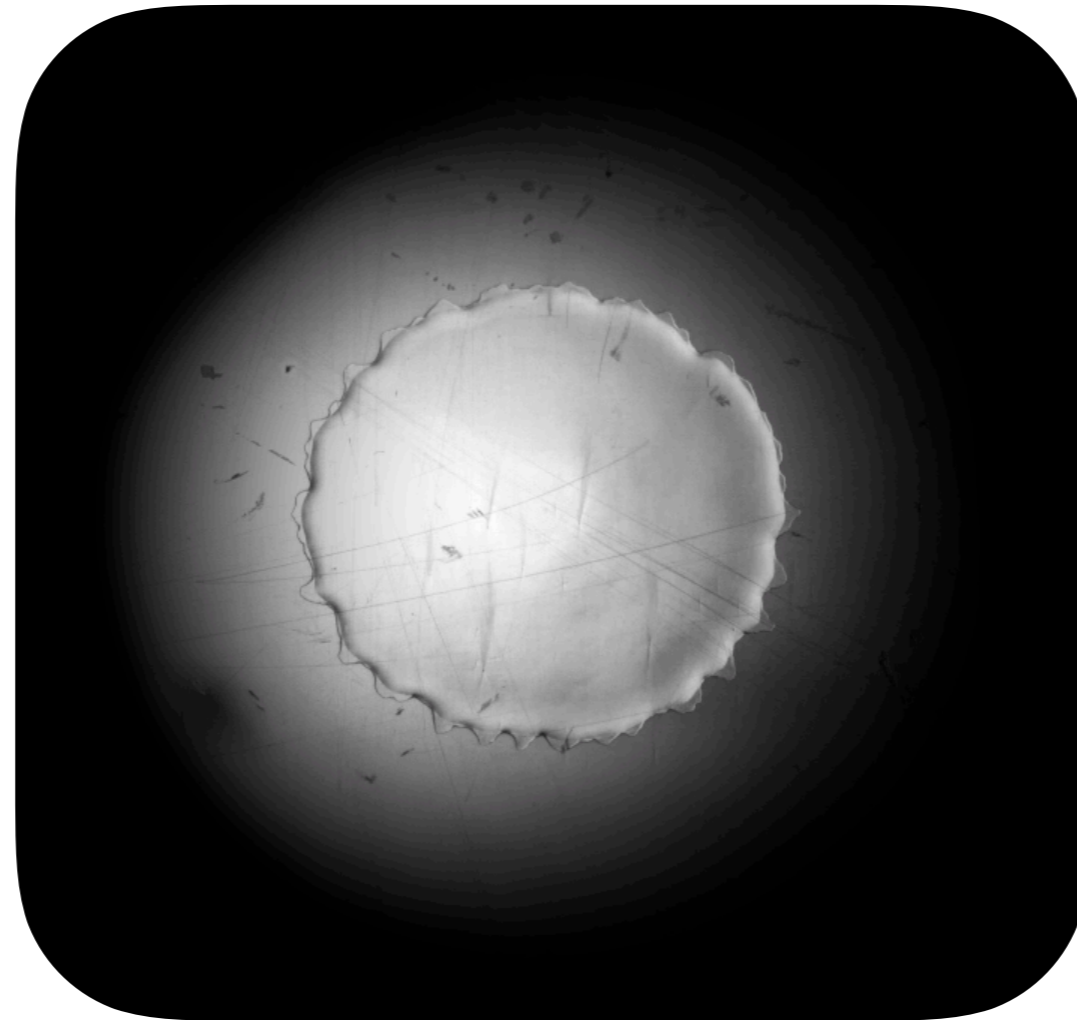


THE FROZEN PATTERNS

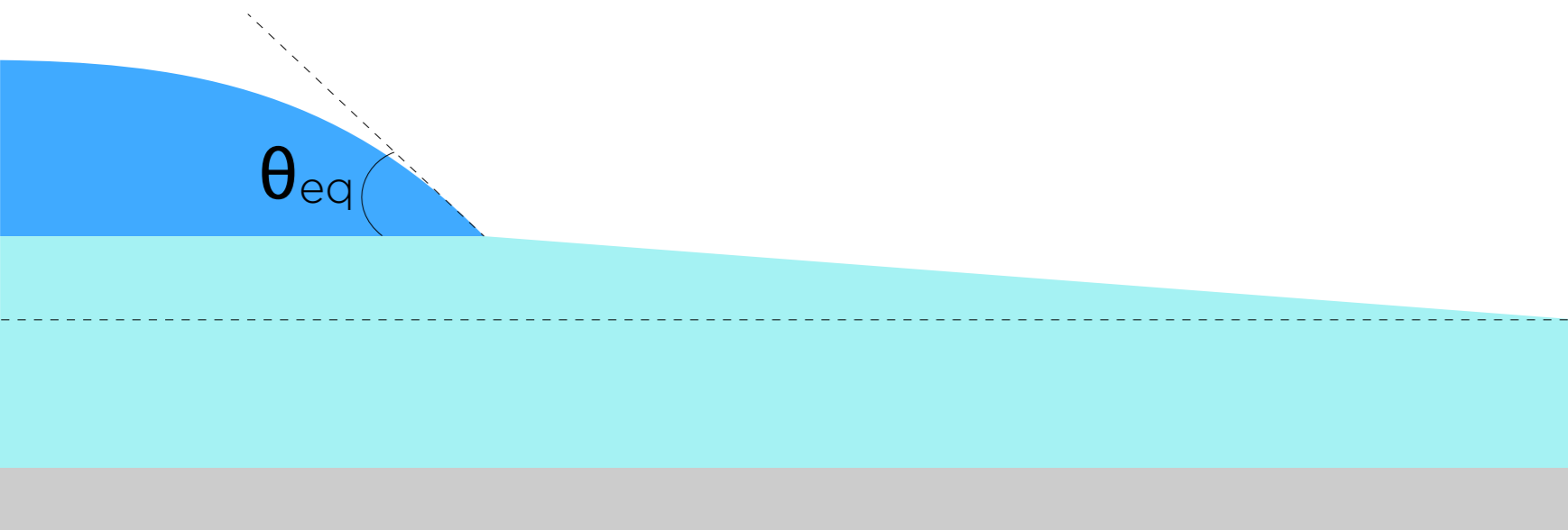


● The different patterns are a consequence of the competition between capillary retraction and solidification

WATER/ICE CONTACT ANGLE

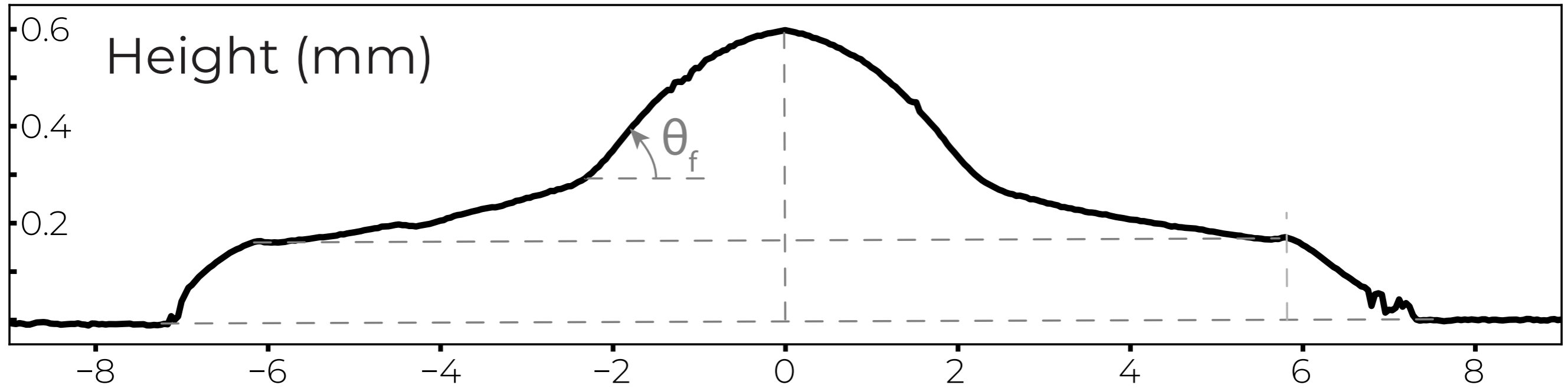


● In the case $\tau_{\text{ret}} < \tau_{\text{sol}}$, water stops retracting when it found its equilibrium shape and contact angle.



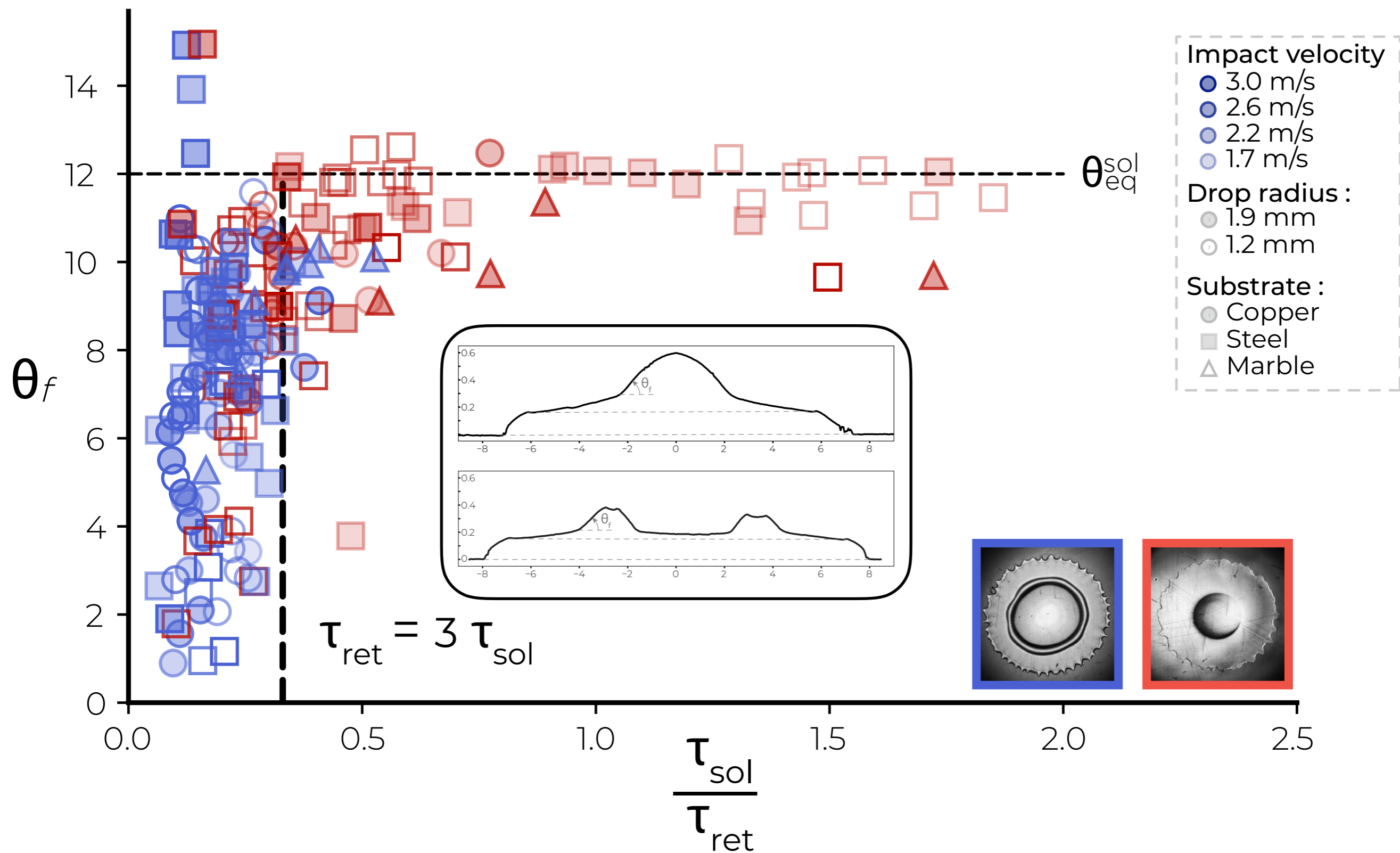
θ_{eq} is expected to be the equilibrium contact angle of water on ice !

HEIGHT PROFILES



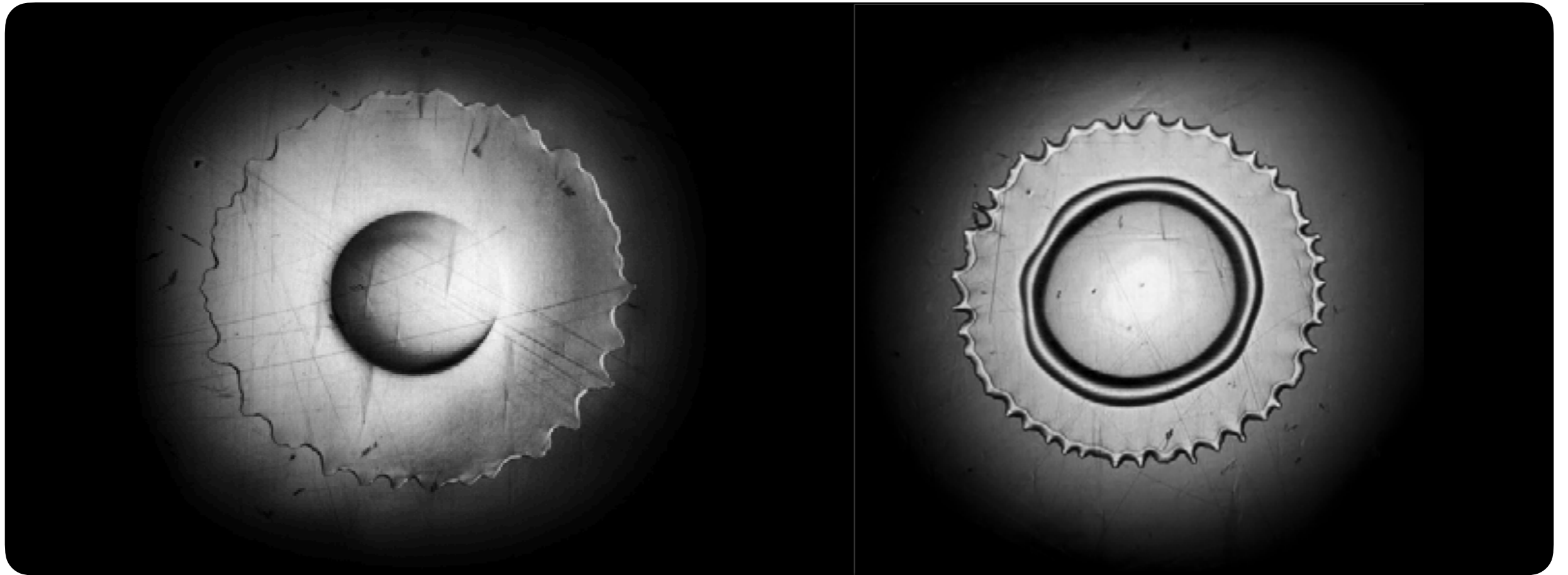
● θ_f is related to the contact angle that water made with ice at the moment it has been frozen.

WATER/ICE CONTACT ANGLE



● θ_f reaches $\theta_{eq}^{sol} = 12^\circ$ which gives an estimation of the equilibrium contact angle of water on ice !

CONCLUSION



- Thermal properties of the substrate strongly influence the freezing dynamics.
- The understanding of the competition between capillary hydrodynamics and solidification is crucial to predict the shape of such a frozen structure.
- This experiment gives an interesting estimation of the equilibrium contact angle of water on ice : 12° .

FINN